G. H. Lee

R. K. Marp

# BEST AVAILABLE COPY

PATERY CLEARANCES

I have given patent clearance to the following documents.

#### Trainer

#### Title

Ho-54-3724 (Copy enclosed)

Correct Methods in Plutonius Foel Fabrication", a 16 am action picture in color and sound.

menuring: Discloses the subject natter of BJIR-377 -ARC Case S-16, 710; BATR-1512 - ARC Case No. 5-27,336; and IMIN-1745 - AEC Case No. 5-31,328. Patent applications have been filed on AEC Cases 3-16,710 and 3-27,336. ASC Came 3-31,328 has been inactivated.

BY-61.602 (Copy enclosed)

Correctes Research and Development Justiarly Report - July -September 1964

Remarks: Discloses the subject matter of BAIR-123 -ABC Come 3-24,036; BATR-1533 - ABC Come 3-27,443; BATH-1616 - ARC Case 3-20,267; BATH-1644 - ARC Case 5-29,355; and BATR-1745 - ASC Case 5-31,328. ARK Case 3-24,000 has been combined with ARC Case S-22,961 (BSTR-1209) and patented. ABC Came S-27,443 and 5-31,328 have been inactivated. Patent applications have been filed on ARC Cases 3-28,207 and 3-29,355.

RE CE

Enclosures: HW-SA-3724 HW-81602

Reviewed and Approved for Public Release by the Hanford **Declassification Project** W.F. Nicaise PNNL ADD 4-5-2000 Date

**#** }.

| TITLE   |  | DOCUMENT NUMBER        |
|---|--|------------------------|
| CERAMICS RESEARCH AND DEVILOPMENT UNIX - SEPTEMBER 1964 | ARTERLY REPORT   | Hw-31602               |
| AUTHOR  |  |                        |
| PROPOSED DISTRIBUTION TTD-4500                          |  |                        |
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| REMARKS: INTR-1207 combined with IN                     | R-1209 and patented. 1MD   | R-1533 and BWIR-1745   |
| have been dropped. Patent applicati                     | ons have been filed On Hw  | 18-1616 and BWIR-1644. |
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| Publications File                                       |  |                        |
|   | Robert Keith Sharp   |                        |
|   | PATENT ATTORNEY COUNSEL'S OFFICE   |                        |
|   |  |                        |

G. R. Lee, Chief Chicago Patent Group February 24, 1965

S. K. Sherp, Patent Attorney Chicago Petent Group

HWIH-1207 - ABC CASE S-24,036 HWIH-1523 - ABC CASE S-27,443 HWIH-1616 - ABC CASE S-20,267 HWIH-1644 - ABC CASE S-29,355 HWIH-1745 - ABC CASE S-31,328

I have given patent clearance on the following document, which you have received under standard distribution. The subject matter of the above cases is disclosed.

IN-31602 - CERANICS RESEARCH AND DEVELOPMENT QUARTERLY REPORT JULY - SEPTEMBER 1964

HWIR-1287 - ARC Case 8-24,086 has been combined with HWIR-1209 - ARC Case 8-22,961 and patented.

HAIR-1533 - AEC Case 3-27,443 has been dropped.

Patent applications have been filed on the other cases.

Material directed to HAR-1735 - AEC Case 9-31,296 was refused clearance and resoved before printing.

MES: eg

cc: RC Emais

HAIR Files

COMPANY

RICHLAND, WASHINGTON . . . TELEPHONE AREA CODE 509, 942-1111

Extension 3601

HANFORD

ATOMIC

PRODUCTS

OPERATION

3760 Bldg., 300 Area

Hoverbox 17, 1904

Mr. George H. Lee, Chief Chicago Patent Group U. S. Atomic Energy Commission Chicago Operations Office 9800 South Cass Avenue Argonne, Illinois

Subject: RELEASE OF DOCUMENT

bec: BVIR Files

Publications File

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LB

| HWIR-               | AEC CASE NO.         |
|---------------------|----------------------|
| 1533<br>1 <b>04</b> | 3-27,143             |
| 1732                | 5-29,355<br>8-31,293 |
| 1745                | 9-31-320             |

Dear Mr. Lee:

In accordance with your letters of April 8, 1960 and July 18, 1961, I have given patent clearance for distribution or publication of the following document, a copy of which is enclosed:

Document Number: propos

Title: Cermics Research and Davelogment Operation quarterly

Author: Report" - April - June, 1964.

Type of Distribution: 2770-4500

The above invention report(s) is (are) involved.

Remarks: A potent application has been filed on ABC Case 9-29,355. The

other cases have been dropped.

Very truly yours,

Robert Keith Sharp Patent Attorney

RKS:eg Enclosure

cc: Roland A. Anderson - USAEC-HDQ (w/encl.)

| TITLE   | DOCUMENT NUMBER              |
|---|------------------------------|
| CERAMICS RESEARCH AND DEVELOPMENT OPERATION QUART<br>APRIL - JUNE, 1964 | ERLY REPORT<br>BW-31601      |
| AUTHOR  |                              |
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| PATENT ATTOR  |                              |
| COUNSEL'S OF  | FICE                         |
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Extension 3601

HANFORD

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3760 Bldg., 300 Area

NOV 1 0 1964

bcc: HWIR-1533

HWIR-1644

Publications File

Record Copy

LB

Mr. George H. Lee, Chief Chicago Patent Group U. S. Atomic Energy Commission Chicago Operations Office 9800 South Cass Avenue Argonne, Illinois

Subject: RELEASE OF DOCUMENT

HWIR-

AEC CASE NO.

1533

S-27,443

1644

3-29,355

Dear Mr. Lee:

In accordance with your letters of April 8, 1960 and July 18, 1961, I have given patent clearance for distribution or publication of the following document, a copy of which is enclosed:

Document Number: None

Title: "Plutonium R&D Newsletter - Reporting Results for July,

August and September, 1964 - Issue No. 7"

Author: J. V. McMaster

Type of Distribution: Special

The above invention report(s) xxx(are) involved.

Remarks: AEC Case S-27,443 has been dropped. A patent application has

been filed on AEC Case S-29,355.

Very truly yours,

Robert Keith Sharp Patent Attorney

RKS: eg

Enclosure

cc: Roland A. Anderson - USAEC-HDQ (w/encl.) A PRIME CONTRACTOR FOR THE U.S. ATOMIC ENERGY COMMISSION

|     | McMaster |
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| TO: | <br>     |

| TITLE  | DOCUMENT NUMBER                       |
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| PLUTONIUM RAD NEWSLETTER - Reporting Results for July,<br>August and September, 1984 - ISSUE NO. 7 | None                                  |
| AUTHOR   |                                       |
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| AUTHOR (Staff)   | 1                  |
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# UNITED STATES ATOMIC ENERGY COMMISSION

WASHINGTON 25, D.C.

February 11, 1963

GCP:RAA

Mr. Robert Keith Sharp Patent Attorney General Electric Company 3760 Building, 300 Area Richland, Washington

SUBJECT: AEC CASE S-27,443 (HWIR NO. 1533)

Dear Mr. Sharp:

There was transmitted to this office with Mr. Lee's memorandum of August 9, 1962, your letter and the above HVIR disclosure. This office has determined that it is not advisable for the Government to proceed with the preparation of a patent application on this case since the thermal treatment of uranium dioxide in the presence of hydrogen, steam, and moist gases is old as can be seen from: (1) the article by Arenberg and Jahn on pages 179 to 183 of volume 41 of the Journal of the American Ceranic Society; (2) NP-6667; (3) NP-8383; and (4) British Patent 844,980. All of these references are abstracted in Nuclear Science Abstracts.

Very truly yours,

Roland A. Anderson Assistant General Counsel

and a. amolo

for Patents

cc: George H. Lee, Chief Chicago Patent Group

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# DETERMINATION OF NITROGEN AS URANIUM NITRIDES IN FUSED URANIUM DIOXIDE (UO2)

By Harlan J. Anderson and James C. Langford

Hanford Atomic Products Operation General Electric Company Richland, Washington \*

#### Introduction

In-reactor tests of  $UO_2$  fuel elements can be abruptly terminated by cladding failures caused by excessive internal gas pressures. In fuel fabrication development studies, therefore, an accurate analysis is required of fixed or sorbed gases present in candidate fuel materials before fabrication  $(\frac{1}{2})$ . Fused  $UO_2$  is one of several candidate ceramic fuel materials.

Brite and Anderson reported (3) the presence, ease of formation, and possible mechanism of formation of uranium nitrides in fused  $UO_2$ . Anderson also reported  $(\frac{1}{4})$  that uranium mononitride (UN), uranium sesquinitride  $(U_2N_3)$ , and uranium dinitride  $(UN_2)$  can act as copious sources of nitrogen in fused  $UO_2$ .

In our laboratories, vacuum extraction and Kjeldahl techniques are used to analyze for fixed or sorbed gas content in UO2 samples. Past efforts to correlate nitrogen values obtained by these two analytical techniques with calculated values of prepared  $\rm UO_2$  samples containing known amounts of UN and  $\rm UN_2$  have not been successful. Nitrogen values for samples of commercially fused  $\rm UO_2$  also have represented areas of disagreement between vendor and our laboratories. Because of inconsistency among analyses, study of analytical techniques was undertaken and completed.

A new analytical technique was developed and successfully used to analyze the nitrogen content (UN,  $U_2N_3$ ,  $UN_2$ ) in fused  $UO_2$ .

<sup>\*</sup> Work performed for the U. S. Atomic Energy Commission under Contract AT(45-1)-1350.

#### Abstract

A new Kjeldahl digestion technique that uses a mixture of 1:1 diluted hydrochloric acid with additions of copper selenate and hydrofluosilicic acid was successfully used to analyze the nitrogen content (UN,  $U_2N_3$ ,  $UN_2$ ) in fused uranium dioxide ( $UO_2$ ). Usual digestion techniques and vacuum extraction at  $1000^{\circ}$ C were inadequate for analysis of all uranium nitride species present in (fused)  $UO_2$ .

#### General Approach

Our observations and data showed that the bulk of the nitrogen present in fused  $\mathrm{UO}_2$  is in the form of uranium nitrides. The Kjeldahl technique, therefore, appeared to be the best analytical approach. Dissolution of  $\mathrm{UO}_2$  samples was considered of primary importance.

Reagents that might be effective in dissolving  $\mathrm{UO}_2$  have been reported (2). Determinations of nitrogen in  $\mathrm{UO}_2$  has been reported (7) by Bennett using an oxidizing alkaline fusion followed by measurement of the volume of released nitrogen. Generally, the analytical approach for nitrogen determination was the Kjeldahl method with modifications of digestion techniques (8). A note (5) on a method for the determination of nitrogen content in uranium nitrides was important since these nitrogen species were identified as present in our fused  $\mathrm{UO}_2$ . Several digestion methods were tested using 200 milligrams (mg) samples of -100 mesh  $\mathrm{UO}_2$ . Two prepared samples consisting of UN in  $\mathrm{UO}_2$  and  $\mathrm{UN}_2$  in  $\mathrm{UO}_2$  were used for each method.

Existing routine methods used in our laboratories yielded poor results on both UN and UN<sub>2</sub> content in UO<sub>2</sub> prepared samples. One method consisted of sample digestion in concentrated HCl, or variations of diluted HCl with additions of zinc metal for generation of active hydrogen. Another method was a sample digestion in HGlO<sub>h</sub> and  $H_2O_2$  or Na<sub>2</sub>O<sub>2</sub>.

Only nitrogen values obtained by digestion of the samples in a mixture consisting of 1:1 diluted HCl with additions of copper selenate and hydrofluosilicic acid were acceptable for both UN in UO<sub>2</sub> and UN<sub>2</sub> in UO<sub>2</sub> prepared samples.

#### Apparatus and Reagents

Kjeldahl equipment, conventional laboratory glassware, and reagent grade chemicals were used unless otherwise stated.

A NaOH solution was made by dissolving 680 grams of NaOH in two liters of distilled water. Devarda's alloy, 0.5 grams, was added. Solutions were boiled until the volume was reduced to 1.8 liters (2). A mixed indicator of brom cresol green (6) and methyl red was used. Methyl red indicator was used to increase the sensitivity of the end point direction.

#### Procedure

Weigh out about 200 mg. of -100 mesh UO<sub>2</sub> sample into a 50 ml. Erlenmeyer flask. Record actual weight. Then, add 25 ml. of 1:1 HCl and 2 ml. of H<sub>2</sub>SiF<sub>6</sub>. Do not cover, but heat just below boiling for about 30 minutes. Add about 200 mg. of copper or potassium selenate. Digest until solution is complete.

Transfer the cooled sample solution to Kjeldahl distillation equipment and add 25 ml. NaOH solution. Distill and collect the condensate in a 50 ml. Erlenmeyer flask containing the mixed indicator solution and 5 ml. of 4% boric acid solution (6). Adjust the heat input so that about 20 ml. of condensate will be collected in five minutes. The boric acid solution need not be accurately measured (9).

Titrate the collected ammonia (ammonium borate) with a standard acid of 0.005 normality ( $\underline{N}$ ). Make a blank determination using the same amount of reagent as in the sample determination.

Calculate nitrogen content by the following formula:

parts per million (ppm) N (nitrogen) = (ml Titration - ml Blank) x N x 14.007 x 1000

Grams Sample

Duplicate results should agree within 0.3% relative.

#### Results and Discussion

The preliminary work was performed on two samples consisting of UN in UO<sub>2</sub> and UN<sub>2</sub> in UO<sub>2</sub>. Table 1 shows that of the several digestion techniques available for analyzing nitrogen as uranium nitrides in UO<sub>2</sub>, only the recommended technique gave complete recovery of the nitrogen. An important feature of this digestion

technique is the essential action of the selenate ion, described by Lathouse et al(5).

Past efforts to correlate nitrogen values obtained by vacuum extraction and by Kjeldahl techniques were not successful on either commercial samples or prepared samples (Table I) containing known amounts of UN and UN2 in UO2.

An analysis of results indicated that the analytical techniques used were biased toward particular species of uranium nitride. Some digestion procedures using Kjeldahl techniques gave good values for fused UO<sub>2</sub> containing UN, but were erratic for UN<sub>2</sub> in UO<sub>2</sub>. In contrast, the vacuum extraction technique at 1000°C gave good results for UN<sub>2</sub> and U<sub>2</sub>N<sub>3</sub>, but low results for UN in UO<sub>2</sub>. UN is reportedly stable in vacuum to about 1700°C.

Vacuum extraction techniques, of course, remain quite useful for measurements of sorbed gases that are released from UO<sub>2</sub> at the generally used 1000°C extracting temperature. But for fused UO<sub>2</sub> that contains UN or other high temperature stable compounds, a new, high vacuum, high temperature technique is needed.

We have modified high temperature vacuum fusion equipment to permit operating temperatures to 2000°C. Ordinarily a graphite crucible and graphite heat shield is used. Graphite reduces UO<sub>2</sub> at 2000°C. That reaction may be useful as an analytical technique for determining oxygen-to-uranium atom ratios. Use of a tungsten crucible and tungsten powder for a heat shield in our vacuum fusion equipment appears to be a promising analytical technique for high temperature compounds such as UN in UO<sub>2</sub>.

#### Conclusions

Existing routine digestion techniques for Kjeldahl analysis, and vacuum extraction techniques for analysis of all uranium nitride species present in fused  ${\rm UO}_2$ , were inadequate. A satisfactory technique was developed and successfully used.

From our studies on the ease of formation of uranium nitrides in fused  ${\rm UO}_2$ , we conclude that uranium nitride formations may also occur in  ${\rm UO}_2$  powders and pellets that are sintered in cracked ammonia. Use of pure hydrogen rather than cracked ammonia in  ${\rm UO}_2$  sintered processes is recommended.

#### Acknowledgement

The authors thank both Mrs. I. S. Paret and Mrs. A. D. Couch for performing many developmental determinations. Thanks are also due to D. W. Brite, and D. R. de Halas and W. E. Roake for their helpful criticisms and suggestions.

#### Literature Cited

- (1) Anicetti, R. J., Hauth, J. J. "Specifications for Fused Uranium Dioxide", HW-61653 Rev. 1. February 15, 1961.
- (2) Belle, J. (Ed.). "Uranium Dioxide" Properties and Nuclear Application, (USAEC, 1961)
- (3) Cadwell, J. J. "Quarterly Progress Report", Fuels Development Operation,
  HW-72346 October, November, December, 1961 (Classified)
- (4) Cadwell, J. J., "Quarterly Progress Report", Fuels Development Operation,
  HW-74377 April, May. June, 1962 (Classified)
- (5) Lathouse, Joan, Huber, F. E. Jr., Chase, B. L. Analytical Chemistry, Vol. 31, December 9, 1959, page 1606-7
- (6) Pierce W. C., Haenisch, E. L., "Quantitative Analysis", 2nd ed., page 123
  Wiley, New York, 1940
- (7) Popper, P., (Ed.) <u>Special Ceramics</u>, Proceedings of a Symposium, British Ceramic Research Association, Heywood, London, 1960
- (8) Rodden, C. J., "Analytical Chemistry of the Manhattan Project", page 208, McGraw Hill, New York, 1950
- (9) Winkler, L. W., Z. angew Chem., 26, page 231 (1913)

TABLE I. Analysis of Nitrogen as Uranium Nitrides in Fused  ${\rm UO}_2$ 

|  | Nitroger |      |            | Nitrogen (ppm) |             |  |  |  |
|--|----------|------|------------|----------------|-------------|--|--|--|
| Sample                                 | 1_       | 2    | <u> 3b</u> | 14             | Theoretical |  |  |  |
| UN (in UO <sub>2</sub> )               | 690      | 890  | 1310       | 250            | 1340        |  |  |  |
| UN <sub>2</sub> (in UO <sub>2</sub> )ª | 540      | 1450 | 1220       | 690            | 1250        |  |  |  |

## Digestion Methods (Kjeldahl Techniques)

- 1. Hydrochloric Acid
- 2. Perchloric Acid and Hydrogen Peroxide
- 3. 1:1 HCl with additions of (copper) selenate and hydrofluosilicic acid.
- 4. Vacuum Extraction at 1000°C with mass spectrometric analysis of gases.
- Some U2N3 possible in sample
- b New Digestion Technique

# DETERMINATION AND CONTROL OF NITROGEN AS URANIUM NITRIDES IN FUSED URANIUM DIOXIDE (UO2)

BY Harlan J. Anderson and James C. Langford

Hanford Atomic Products Operation General Electric Company Richland, Washington\*

#### Introduction

In-reactor tests of  $\mathrm{UO}_2$  fuel elements can be abruptly terminated by cladding failures caused by excessive internal gas pressures. In fuel fabrication development studies, therefore, an accurate analysis is required of fixed or sorbed gases present in candidate fuel materials before fabrication  $(\frac{1}{2})$ . Fused  $\mathrm{UO}_2$  is one of several candidate ceramic fuel materials.

Brite and Anderson reported (3) the presence, ease of formation, and possible mechanism of formation of uranium nitrides in fused  $UO_2$ . Anderson also reported (4) that uranium mononitride (UN), uranium sesquinitride ( $U_2N_3$ ), and uranium dinitride ( $UN_2$ ) can act as copious sources of nitrogen in fused  $UO_2$ .

In our laboratories, vacuum extraction and Kjeldahl techniques are used to analyze for fixed or sorbed gas content in UO<sub>2</sub> samples. Past efforts to correlate nitrogen values obtained by these two analytical techniques with calculated values of prepared UO<sub>2</sub> samples containing known amounts of UN and UN<sub>2</sub> have not been successful. Nitrogen values for samples of commercially fused UO<sub>2</sub> also have represented areas of disagreement between vendor and our laboratories. Because of inconsistency among analyses, study of analytical techniques was undertaken and completed.

A new analytical technique was developed and successfully used to analyze the nitrogen content (UN, U2N3, UN2) in fused UO2.

<sup>\*</sup> Work performed for the U. S. Atomic Energy Commission under Contract AT(45-1)-1350.

#### Abstract

A new Kjeldahl digestion technique that uses a mixture of 1:1 diluted hydrochloric acid with additions of copper selenate and hydrofluosilicic acid was successfully used to analyze the nitrogen content (UN, U<sub>2</sub>N<sub>3</sub>, UN<sub>2</sub>) in fused uranium dioxide (UO<sub>2</sub>). Usual digestion techniques and vacuum extraction at 1000°C were inadequate for analysis of all uranium nitride species present in (fused) UO<sub>2</sub>. An important adjunct to these studies showed that high nitrogen levels in UO<sub>2</sub> can be reduced to acceptable levels by heat treating bulk UO<sub>2</sub> supplies at 1750°C in moist hydrogen.

#### General Approach

Our observations and data showed that the bulk of the nitrogen present in fused  $\mathrm{UO}_2$  is in the form of uranium nitrides. The Kjeldahl technique, therefore, appeared to be the best analytical approach. Dissolution of  $\mathrm{UO}_2$  samples was considered of primary importance.

Reagents that might be effective in dissolving  $UO_2$  have been reported (2). Determinations of nitrogen in  $UO_2$  has been reported (7) by Bennett using an oxidizing alkaline fusion followed by measurement of the volume of released nitrogen. Generally, the analytical approach for nitrogen determination was the Kjeldahl method with modifications of digestion techniques (8). A note (5) on a method for the determination of nitrogen content in uranium nitrides was important since these nitrogen species were identified as present in our fused  $UO_2$ . Several digestion methods were tested using 200 milligrams (mg) samples of -100 mesh  $UO_2$ . Two prepared samples consisting of UN in  $UO_2$  and  $UO_3$  in  $UO_4$  were used for each method.

Existing routine methods used in our laboratories yielded poor results on both UN and UN<sub>2</sub> content in UO<sub>2</sub> prepared samples. One method consisted of sample digestion in concentrated HCl, or variations of diluted HCl with additions of zinc metal for generation of active hydrogen. Another method was a sample digestion in HClO<sub>h</sub> and H<sub>2</sub>O<sub>2</sub> or Na<sub>2</sub>O<sub>2</sub>.

Only nitrogen values obtained by digestion of the samples in a mixture consisting of 1:1 diluted HCl with additions of copper selenate and hydrofluosilicic acid were acceptable for both UN in UO<sub>2</sub> and UN<sub>2</sub> in UO<sub>2</sub> prepared samples.

#### Apparatus and Reagents

Kjeldahl equipment, conventional laboratory glassware, and reagent grade chemicals were used unless otherwise stated.

A NaOH solution was made by dissolving 680 grams of NaOH in two liters of distilled water. Devarda's alloy, 0.5 grams, was added. Solutions were boiled until the volume was reduced to 1.8 liters (9). A mixed indicator of brom cresol green (6) and methyl red was used. Methyl red indicator was used to increase the sensitivity of the end point direction.

#### Procedure

Weigh out about 200 mg. of -100 mesh UO<sub>2</sub> sample into a 50 ml. Erlenmeyer flask. Record actual weight. Then, add 25 ml. of 1:1 HCl and 2 ml. of H<sub>2</sub>SiF<sub>6</sub>. Do not cover, but heat just below boiling for about 30 minutes. Add about 200 mg. of copper or potassium selenate. Digest until solution is complete.

Transfer the cooled sample solution to Kjeldahl distillation equipment and add 25 ml. NaOH solution. Distill and collect the condensate in a 50 ml. Erlenmeyer flask containing the mixed indicator solution and 5 ml. of 4% boric acid solution (6). Adjust the heat input so that about 20 ml. of condensate will be collected in five minutes. The boric acid solution need not be accurately measured (9).

Titrate the collected ammonia (ammonium borate) with a standard acid of 0.005 normality ( $\underline{N}$ ). Make a blank determination using the same amount of reagent as in the sample determination.

Calculate nitrogen content by the following formula:

parts per million (ppm) N (nitrogen) =  $\frac{\text{(ml Titration - ml Blank)} \times N \times 14.007 \times 1000}{\text{Grams Sample}}$ Duplicate results should agree within 0.3% relative.

#### Results and Discussion

The preliminary work was performed on two samples consisting of UN in UO<sub>2</sub> and UN<sub>2</sub> in UO<sub>2</sub>. Table 1 shows that of the several digestion techniques available for analyzing nitrogen as uranium nitrides in UO<sub>2</sub>, only the recommended technique gave complete recovery of the nitrogen. An important feature of this digestion

technique is the essential action of the selenate ion, described by Lathouse et al(5).

Past efforts to correlate nitrogen values obtained by vacuum extraction and by Kjeldahl techniques were not successful on either commercial samples or prepared samples (Table 1) containing known amounts of UN and UN2 in UO2.

An analysis of results indicated that the analytical techniques used were biased toward particular species of uranium nitride. Some digestion procedures using Kjeldahl techniques gave good values for fused UO<sub>2</sub> containing UN, but were erratic for UN<sub>2</sub> in UO<sub>2</sub>. In contrast, the vacuum extraction technique at 1000°C gave good results for UN<sub>2</sub> and U<sub>2</sub>N<sub>3</sub>, but low results for UN in UO<sub>2</sub>. UN is reportedly stable in vacuum to about 1700°C.

Vacuum extraction techniques, of course, remain quite useful for measurements of sorbed gases that are released from UO<sub>2</sub> at the generally used 1000°C extracting temperature. But for fused UO<sub>2</sub> that contains UN or other high temperature stable compounds, a new, high vacuum, high temperature technique is needed.

We have modified high temperature vacuum fusion equipment to permit operating temperatures to 2000°C. Ordinarily a graphite crucible and graphite heat shield is used. Graphite reduces UO<sub>2</sub> at 2000°C. That reaction may be useful as an analytical technique for determining oxygen-to-uranium atom ratios. Use of a tungsten crucible and tungsten powder for a heat shield in our vacuum fusion equipment appears to be a promising analytical technique for high temperature compounds such as UN in UO<sub>2</sub>.

#### Removal of Impurities

An important adjunct to these studies showed that high nitrogen levels in fused UO<sub>2</sub> can be reduced to acceptable levels by heat treating bulk UO<sub>2</sub> materials at 1750°C in moist hydrogen.

Fused UO<sub>2</sub> samples originally containing UN and UN<sub>2</sub> were examined after heat treating at 1750°C for 12 hours in moist (1000 ppm H<sub>2</sub>0) hydrogen. Ceramographic examination and nitrogen analysis by the new digestion technique showed removal of about 80% of the nitrogen content (Table II). Uranium nitrides (UN, U<sub>2</sub>N<sub>3</sub>, UN<sub>2</sub>) can thus be substantially removed by this process.

#### Conclusions

Existing routine digestion techniques for Kjeldahl analysis, and vacuum extraction techniques for analysis of all uranium nitride species present in fused  ${\rm UO}_2$ , were inadequate. A satisfactory technique was developed and successfully used.

From our studies on the ease of formation of uranium nitrides in fused  ${\rm UO}_2$ , we conclude that uranium nitride formations may also occur in  ${\rm UO}_2$  powders and pellets that are sintered in cracked ammonia. Use of pure hydrogen rather than cracked ammonia in  ${\rm UO}_2$  sintered processes is recommended.

#### Acknowledgement

The authors thank both Mrs. I. S. Parent and Mrs. A. D. Couch for performing many developmental determinations. Thanks are also due to D. W. Brite, and D. R. de Halas and W. E. Roake for their helpful criticisms and suggestions.

#### Literature Cited

- (1) Anicetti, R. J., Hauth, J. J. "Specifications for Fused Uranium Dioxide", HW-61653 Rev. 1. February 15, 1961.
- (2) Belle, J. (Ed.). "Uranium Dioxide" Properties and Nuclear Application, (USAEC, 1961)
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TABLE I. Analysis of Nitrogen as Uranium Nitrides in Fused UO2

|                                  |     | Nitrog | en (ppm)    |     |             |
|----------------------------------|-----|--------|-------------|-----|-------------|
| Sample                           | 1   | 2      | <u> 3</u> b | 14  | Theoretical |
| UN (in UO <sub>2</sub> )         | 690 | 890    | 1310        | 250 | 1340        |
| $UN_2 (in UO_2)^{\underline{a}}$ | 540 | 1450   | 1220        | 690 | 1250        |

## Digestion Methods (Kjeldahl Techniques)

- 1. Hydrochloric Acid
- 2. Perchloric Acid and Hydrogen Peroxide
- 3. 1:1 HCl with additions of (copper) selenate and hydrofluosilicic acid.
- 4. Vacuum Extraction at 1000°C with mass spectrometric analysis of gases.
- Some U2N3 possible in sample
- b New Digestion Technique

TABLE II. Removal of Nitrogen from Fused UO2

# Nitrogen (ppm)

| Sample                                | Before |           | After (H <sub>2</sub> Treatment) |
|---------------------------------------|--------|-----------|----------------------------------|
|                                       |        | Kjeldahla | Vacuum Extraction - 1000°C       |
| UN (in UO <sub>2</sub> )              | 1310   | 265       | 260                              |
| UN <sub>2</sub> (in UO <sub>2</sub> ) | 1220   | 230       | 388                              |

a Using New Digestion Technique

RICHLAND, WASHINGTON . . . TELEPHONE WHItehall 2-1111

HANFORD ATOMIC
PRODUCTS OPERATION

HANFORD LABORATORIES OPERATION

September 10, 1962

Dr. L. T. Hallett, Editor Analytical Chemistry 1155 Sixteenth Street, W. W. Washington 5, D. C.

Dear Dr. Hallett:

# DETERMINATION OF HITROGEN AS URANIUM MITRIDES IN FUSIO GRANIUM DICKIDS

Attached are the required copies of our manuscript HW-5A-2063 for publication purposes.

The information, we feel, is most important to the continued progress of both national and international  $w_{ij}$  fuel power programs. Both national and foreign locations have contacted me about use of our technique to provide new information on their in-reactor fuel element failures. We feel, therefore, that the information should be presented immediately for consideration and primarily for analytical personnel.

Earlier release of the information was delayed. A section of the original manuscript was removed pending possible patent application. When this information becomes available, I would like to forward a section about the control of impurities. At this time, we are in a position to present this manuscript for your consideration.

Sincerely yours,

CFIGINAL SIGNED BY
H. J. ANDERSON

H. J. Anderson Cerumic Fuels Development Hanford Laboratories

db: ALE

cc: JC Langford

A PER SHETE ONTRACTOR FOR THE U.S. ATOMIC ENERGY COMMISSION

September 12, 1962

Mr. George H. Lee, Chief Chicago Patent Group U. S. Atomic Energy Commission Chicago Operations Office 9800 South Cass Avenue Argonne, Illinois

### BITR-1533 - AEC CASE 13-27,443

Dear Mr. Lee:

For your information, I am enclosing the re-written version of BN-SA-2663 - "Determination of Mitrogen as Uranium Mitrides in Fused UO2 by Harlen J. Anderson and James C. Langford - referred to in my letter of August 29, 1962, to which I have given clearance.

Very truly yours,

Robert Keith Sharp Patent Attorney

RKS; eg

Enclosure

Roland A. Anderson - USAEC-HDQ.

bec: HVIR-1533 Record Copy

Publications File

| TITAL   |  | DOCUMENT NUMBER                       |
|---|--|---------------------------------------|
| DETERMINATION OF NITROGEN AS<br>UO <sub>2</sub> | URANIUM NITRIDES IN FUSED  | HW-SA-2663                            |
| AUTHOR  Harlan J. Anderson and James            | es C. Langford   | · · · · · · · · · · · · · · · · · · · |
| PROPOSED DISTRIBUTION For publication:          | ANALYTICAL CHEMISTRY JOURNAL   |                                       |
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| HWIR-1533                                       | Robert Keith Shar  | <b>)</b>                              |
|   | PATENT ATTORNEY COUNSEL'S OFFICE   | ·<br>!                                |
|   |  |                                       |

August 29, 1960

Mr. George H. Lee, Chief Chicago Patent Group U. S. Atomic Energy Commission Chicago Operations Office 9800 South Cass Averse Argonne, Illinois

## MIR-1533 - AEC CASE 8-27.443

Dear Mr. Lee:

The author has rewritten BN-8A-2663 to eliminate the disclosure relative to this invention.

Very truly yours,

Robert Keith Sharp Patent Attorney

RKS: eg

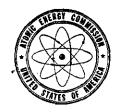
cc: R. A. Anderson - USANC-HDJ.

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Publications File

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| TITLE  | DOCUMENT NUMBER     |  |
|--|---------------------|--|
| DETERMINATION AND CONTROL OF NITROGEN AS URAN  | RIM NTTRIDES        |  |
| IN FUSED URANIUM DIOXIDE (UO2)   | IM-3A-2663          |  |
| AUTHOR   |                     |  |
| H. J. Inderson and James J. Langford   |                     |  |
| PROPOSED DISTRIBUTION For publication in ANALYTICAL CHEMISTRY  |                     |  |
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| REMARKS: Clearance is denied for the present by AEC. Can be eleared if section   |                     |  |
| on "Removal of Impurities" and Table II are deleted.   |                     |  |
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| cc: HWIR-1533 Rober  | t Keith Sharn       |  |
| Publications File PATENT   | ATTORNEY L'S OFFICE |  |
| COUNSE   | 3 011102            |  |



# UNITED STATES ATOMIC ENERGY COMMISSION CHICAGO OPERATIONS OFFICE 9800 South Cass Avenue Argonne, Illinois

August 9, 1962

Mr. Robert Keith Sharp, Patent Attorney Hanford Atomic Products Operation General Electric Company 3760 Building, 300 Area Richland, Washington

HWIR-1533

Subject: PATENT REVIEW OF HW-SA-2663; CASE S-27,443

Dear Mr. Sharp:

Your letter of transmittal for the above case asked for patent clearance on report HW-SA-2663 on an urgent basis. We cannot give clearance for the paper with this material at the present time prior to September 1. Therefore, it would seem that deletions would be required. Since this is an analytical paper, we do not believe this would be too damaging to the paper. If we are able to get an early reply from the Central Office that allows such action, we will immediately give a full release.

Very truly yours,

George H. Lee, Chief Chicago Patent Group



# UNITED STATES ATOMIC ENERGY COMMISSION CHICAGO OPERATIONS OFFICE

9800 South Cass Avenue Argonne, Illinois

August 8, 1962

Mr. Robert Keith Sharp, Patent Attorney Hanford Atomic Products Operation General Electric Company 3760 Building, 300 Area Richland, Washington

Subject:

HWIR-1533

- AEC-S-27,443

HVIR-1534

AEC-S-27,444

Dear Mr. Sharp:

We have assigned the above AEC case number(s) to the invention disclosure(s) which you recently sent to us. Please refer to the above number(s) in all future correspondence.

We will keep you informed as to the status of the above case(s).

Very truly yours,

George H. Lee, Chief Chicago Patent Group

AEC-CH Form 236 (1-61)

H. J. Anderson 325 Bldg. 300 Area

R. J. Andorsti 325 Blag. 300 Area

D. W. Brite 325 Bldg. 300 Area

Your Report of Invention entitled "A Method to Purify Bucker Grade Urantum Dioxide (UO,) Grain" has been designated BVR-1533 and forvarded to the Chicago Patent Group of the Momic Energy Commission for evaluation. It will then be sent by them to the Commission's petent commen in Weshington, D.C.

When the ASC has informed me of its intentions as regards the filing of an application in the U. 5. Petent Office, the information will be communicated to you. In the mountime, please keep se informed as to significant developmental work done in competion with your invention or its actual or contemplated use beyond that described in your Invention Report. This may be done either by a written communication or a rhome call to me.

As I understand it, by iragen treatment to improve the O/V ratio had been used by others. If this is correct, the inclusion of vater vapor becomes the beats for possible putestability. It would, therefore, be deairable to have experimental evidence of the improvement in purification brought about by the inclusion of veter vapor. Also, some indication of the operative range of vater concentration would be desirable.

Patent Attorney

RE Sherp: og 3760 BlAg., 300 Area Phone: 3601

co: BKIR-1533

August 3, 1560

U. 3. Atomic Beargy Commission Chicago Operations Office 9200 Bowth Cass Avenue Argume, Illinois

Attention: Mr. George H. Loe, Chief

Chicago Potent Group

#### Centiemen:

Enclosed berevith are three copies of an invention report, General Electric Case BVER-1503, outitled A Nothed to Purity Buclear Grade Uranium Dioxide (UC<sub>2</sub>) Grain', subsitted by H. J. Anderson, R. J. Anicotti, and D. W. Brite.

The hydrogen treatment of UO, to adjust the O,U ratio has, I understand, been known previously. The point of novelty in the present case is the use of the <u>soist</u> hydrogen. While the limits of water content have not been accurately leterained as yet, the order of magnitude appears to be important. If the ascurt is too low, the impurities are not effectively removed. If it is too high, the O/U ratio is increased.

I understand that what I consider the invention originated by accident. It was observed that an improvement in results had occurred at a time when an assistant had allowed the dehydrating agent treating the hydrogen to become exhausted. The inventors hope to investigate the matter of water concentration in more detail.

References 1-4 are classified.

Two copies of Re-SA-266) - Determination and Control of Ritrogen as Uranium Ritridge in Passed Uranium Dioxide (UC,) are enclosed and alearence is requested for publication in ANALYTICAL CHRISTEY. If

clearance cannot be given promptly (by about September 1, 1962), we would appreciate being informed. The authors would then delete all passages disclosing the subject matter of this invention, thus limiting the paper to the determination of nitrogen.

While the invention is unoits in commection with the FMER, it apparently did not arise specifically under the Flutonius Recycle Progress. I have not sent the disclosure to Mr. Robertson.

Very truly yours,

Robert Kelth Sharp Petent Attorney

AK5:eg

Enclosures

ee: UBAGO-1800 - Att in: Production Division

bec: Record Copy HWIR-1533

LB

# GENERAL ELECTRIC COMPANY

RICHLAND, WASHINGTON

#### REPORT OF INVENTION

A,E,C.CASE NO.

G. E. CASE NO.

HWIR- KS 33

TO: R. K. Sharp

ATTACHED HERETO IS A DESCRIPTION OF WHAT MAY BE AN INVENTION IN:

A method to purify nuclear grade uranium dioxide  $(UO_2)$  grain by heat treating of bulk supplies in a furnace, or a contained reaction vessel, for  $^{14}$ --  $^{16}$  hours at  $800\,^{\circ}$ C -  $^{18}00\,^{\circ}$ C in a (moist  $\approx$  1000 ppm water) hydrogen atmosphere. This method has been reduced to practice by a commercial vendor of  $UO_2$  by following our instructions and specifications. Beneficial results were observed in purity, stoichiometry, density, and crystallinity. (See attached items)

- II: THE NAME, TITLE OR POSITION, WORKS LOCATION, AND PERMANENT ADDRESS OF THE INVENTOR(S) IS:
- H. J. Anderson, Engineer, HAPO., 819 W 23rd Place, Kennewick Washington
- R. J. Anicetti, Specialist, HAPO., 613 Basswood, Richland, Washington
- D. W. Brite, Engineer, HAPO., 403 Smith, Richland, Washington
- III. EVIDENCE AS TO WHEN AND WHERE THE INVENTION WAS MADE CAN BE FOUND IN THE FOLLOWING LISTED WRITTEN OR PICTORIAL MATERIAL (NOTEBOOK, FILE REPORTS OR DRAWINGS, ETC.):
  - 1) CFDO Monthly Report, October, 1961
  - 2) HW-70557, Quarterly Report, April, May, June, 1961 page 5.15
  - 3) HW-72346, Quarterly Report, October, November, December, 1961
  - 4) HW-74377, Quarterly Report, April, May, June 1962
  - 5) HW-SA-2663
  - 6) Memo to E. A. Evans from R. J. Anicetti, May 7, 1962
  - 7) Memo to E. A. Evans from H. J. Anderson, May 31, 1962
- IV: THE APPROXIMATE DATE OF THE FIRST ENTRY IN SAID WRITTEN OR PICTORIAL MATERIAL DESCRIBING OR SHOWING SAID INVENTION IS:

October 1961

V. PERSONS WHO COULD TESTIFY AS TO WHEN AND WHERE THE INVENTION WAS MADE INCLUDE THE FOLLOWING:

W. E. Roake

D. R. de Halas

E. A. Evans TALVANT 7-18-62 HLO - CFDO

NOTE: SUGGESTIONS FOR PREPARING THE INVENTION DESCRIPTION ARE CONTAINED ON THE REVERSE SIDE

accined)

Robert Robert Short

#### Report of Invention

#### Introduction

High density, uranium dioxide grain prepared by fusion or by electrodeposition from fused salt bath contains undesirable inclusions and impurities, such as, uranium metal, uranium carbides, uranium nitrides, and occluded salts. The amount of impurities included in the UO<sub>2</sub> often precludes its use as a muclear fuel.

Ultra-high purity, dense UO2 crystals are also required for basic studies of the properties both in- and ex-reactor. Large crystals, suitable for these studies are most conveniently obtained from UO2 which has been fused in an electric arc furnace.

#### Invention

The chemical and physical properties of highdensity uranium dioxide grain were improved by our method of heat heating UO<sub>2</sub> grain in a furnace for time periods of 4 to 66 hours at 800 --1800 C temperature ranges in a (moist, -1000 ppm water) hydrogen atmosphere.

Briefly, the method consists of the following procedure:

UO2bulk material of various sizes, but normally of -4 +20 mesh, is placed upon a tray with a suitable liner such as molybdenum, and inserted into a cool furnace. The furnace atmosphere is purged with an inert gas such as helium. Hydrogen gas containing moisture of at least 1000 ppm water is

| Short Quiently    | Inventor 7-18-62      | Daniel W. Brite             | 7-18-62   |
|-------------------|-----------------------|-----------------------------|-----------|
| Investor          | Date                  | Inventor                    | Date      |
| Read and Understo | pod for me this 7-18- | Cay of 1962. Witness Willia | n 5. Palu |

admitted into the furnace. Excess hydrogen leaving the furnace is burned by a torch. The temperature is raised 100 - 200 C per hour to operating ranges of 800 - 1800 C but normally at 1750 C. The UO<sub>2</sub> grain remains at temperature for 4 - 66 hours, but normally for 16 hours duration. After turning off the furnace power, the UO<sub>2</sub> grain is cooled at 200 C per hour. When room temperature is attained, the UO<sub>2</sub> grain is removed from the tray and stored.

Both metallic and non-metallic impurities were removed by our method.

The following tables, for examples, illustrate results of use of our method.

TABLE I Ref. HW-70557, April - July, 1961

## UO2 (Fused) Grain

| Item                                       | Before                     | After                  | Remarks           |
|--|----------------------------|------------------------|-------------------|
| O/U atomic ratio                           | 1.96                       | 2.00                   | 4 hours at 1700 C |
| Gas Content<br>CC/gm UO <sub>2</sub> (STP) | 0.09                       | 0.02                   |                   |
| Crystallinity                              | inclusions of 0.06 mm 0.D. | voids of 0.0.0 mm 0.D. |                   |

#### TABLE II

Ref. HW-72346, October - December, 1961

# UO2 (Electrodeposited) Grain

| <u>Ibem</u> | Before     | After          | Remarks            |
|-------------|------------|----------------|--------------------|
| K           | 1400 ppm   | 360 ppm        | 10 hours at 1000 C |
| Pb          | 12,000 ppm | 250 ppm        |                    |
| Cl          | 1100 ppm   | 65 <b>pp</b> m |                    |
| O/U Atomic  | 2.013      | 2.001          |                    |
| ratio       | 27 1-2611  |                |                    |

Robert Anicelle 7/18/62 Maniel W. Bute 7-18-62

Inventor Date

Read and Understood, by me this 7-18/67day of 1962.

Witness Hole Witness William S. Roako

#### TABLE III

Ref. HW-SA-2663, HW-74377, April - June, 1962

## UO2 (Fused) Grain

| <u>Item</u>              | Before   | After   | Remarks            |
|--------------------------|----------|---------|--------------------|
| N (as UN in $UO_2$ )     | 1310 ppm | 265 ppm | 16 hours at 1750 C |
| N (as $UN_2$ in $UO_2$ ) | 1220 ppm | 230 ppm |                    |

#### TABLE IV

Ref. HW-71422, July - September, 1961

### UO2 (High energy impact formed) Grain

| Item    | Before               | After      | Remarks            |
|---------|----------------------|------------|--------------------|
| Density | 90 <b>-</b> 95% T.D. | 99.5% T.D. | 66 hours at 1800 C |

#### Actual Use of Method

This method has been reduced to routine use in our laboratories for improving the purity, density, and crystallinity of UO<sub>2</sub> grain bulk supplies before use in fabrication of reactor fuel test elements. Large single crystals of UO<sub>2</sub> have been treated by this method to improve the chemical and physical properties of specimens useful in fundamental studies.

A commercial vendor has also reduced this method to practice by following our instructions and specifications for a production order of arc fused UO<sub>2</sub>. After arc fusion of UO<sub>2</sub> grain, the material was immediately cooled in hydrogen rather than conventionally cooling the UO<sub>2</sub> in air or

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Witness William 5. Roalu

inert gas such as helium or argon. Chemical and physical properties of  ${\rm UO}_2$  were improved by our hydrogen atmosphere treatment method.

#### Interest in Method

Since this method improves the chemical - physical properties, and thereby enhances the integrity and composition of nuclear fuel materials, such as UO2, that are currently used in pressed, swaged or vibrational compaction manufacturing processes for reactor fuel elements, we feel that important industrial interest is attached to our method. The method is of immediate interest to the USAEC fuels development and reactor programs, to the Hanford Plutonium Recycle Program, to commercial fuel processors such as NUMEC, Kerr-McGee, and Norton Companies, and to foreign countries and organizations such as U.K., Germany, Italy, France, Japan, and Euratom. Attachments:

Read and Understood by me this >-1812 day, 1962.

Witness Alche L. Witness / Milliam S. Rea/co

TO: E. A. EVANS

FROM: R. J. ANICETTI

# FUSED UO2 TREATMENT

During discussions with Norton Company personnel, I recommended a hydrogen atmosphere treatment immediately after arc-fusion to improve crystallinity, density, and stoichiometry. These tests were based upon our experiments conducted by H. J. Anderson, D. W. Brite and myself. Previously, fusions were cooled in air or argon.

cc: HJ Anderson RJ Anicetti letterbook TO: E. A. Evans

FROM: H. J. ANDERSON

# PA

### Fused UO2 Treatment

During discussions on May 28, 1962, with Norton Company personnel, especially Mr. N. Turnbull, I again asked about our tests fro hydrogen atmosphere treatment immediately after arc-fusion of UO<sub>2</sub> to improve crystallinity, density, stoichiometry and to remove impurities (metallic and non-metallic) such as uranium nitrides.

My understanding was that Norton Company would conduct the tests on Run 3 and tell us of the results.

cc: HJ Anderson RJ Anicetti letterbook

# DETERMINATION AND CONTROL OF NITROGEN AS URANIUM NITRIDES IN FUSED URANIUM DIOXIDE (UO2)

By Harlan J. Anderson and James C. Langford

Hanford Atomic Products Operation General Electric Company Richland, Washington\*

#### Introduction

Reactor tests of  ${\rm UO}_2$  fuel elements can be abruptly terminated by cladding failures caused by excessive internal gas pressures. In our fuel fabrication development studies, therefore, an accurate analysis is required of fixed or sorbed gas content present in our fuel candidate materials before fabrication (1). Fused  ${\rm UO}_2$  is one of several candidate ceramic materials used in our studies.

Brite and Anderson have reported (3) on the presence, ease of formation, and possible mechanism of formation of uranium nitrides in fused  $UO_2$ . Anderson has also reported (4) that uranium mononitride (UN), uranium sesquinitride  $(U_2N_3)$ , and uranium dinitride  $(UN_2)$  can act as copious nitrogen suppliers in fused  $UO_2$ .

In our laboratories, vacuum extraction and Kjeldahl techniques are used to analyze for fixed or sorbed gas content in UO<sub>2</sub> samples. Past efforts to correlate nitrogen values obtained by these two analytical techniques with calculated values of prepared samples containing known amounts of UN and UN<sub>2</sub> in UO<sub>2</sub> have not been successful. Nitrogen values for samples of commercial fused UO<sub>2</sub> supplies have also not been in agreement between vendor and our laboratories. Because of this inconsistency among analyses, study of these analytical techniques was under taken and completed.

A new analytical technique was developed and successfully used to analyze the nitrogen content (UN,  $U_2N_3$ ,  $UN_2$ ) in fused  $UO_2$ .

<sup>\*</sup> Work performed for the U.S. Atomic Energy Commission under Contract AT (45 1) 1350.

#### Abstract

A new Kjeldahl digestion technique that uses a mixture of 1:1 diluted hydrochloric acid with additions of copper selenate and hydrofluosilicic acid was successfully used to analyze the nitrogen content (UN, U2N3, UN2) in fused uranium dioxide (UO2). Generally used digestion techniques and vacuum extraction at 1000°C are inadequate for analysis of all uranium nitride species present in (fused) UO2. An important adjunct to these studies showed that high nitrogen levels in UO2 can be reduced to acceptable levels by heat treating bulk UO2 supplies at 1750°C in moist hydrogen.

#### General Approach

Our observations and data showed that the bulk of the nitrogen present in fused UO<sub>2</sub> was present as fixed nitrogen in the form of uranium nitrides. The Kjeldahl technique, therefore, appeared the best approach for solution of our problem. Dissolution of UO<sub>2</sub> samples was considered of prime importance.

Reagents that might be effective in dissolving  $UO_2$  have been reported (2). Determination of nitrogen in  $UO_2$  has been reported (7) by Bennett using a method of oxidizing alkaline fusion followed by measurement of the volume of released nitrogen. Generally, the analytical approach for nitrogen determination was the Kjeldahl method with modifications of digestion techniques (8). A note (5) on a method for the determination of nitrogen content in uranium nitrides was important since these nitrogen species were identified as present in our fused  $UO_2$  supplies.

The Kjeldahl approach was tried with an inclusive digestion technique for uranium nitrides in fused  $\mathrm{UO}_2$ . Several digestion methods were tested using 100 milligrams (mg) samples of -100 mesh  $\mathrm{UO}_2$ . Two prepared samples consisting of UN in  $\mathrm{UO}_2$  and  $\mathrm{UN}_2$  in  $\mathrm{UO}_2$  were used for each method.

Only nitrogen values obtained by digestion of the samples in a mixture consisting of 1:1 diluted HCl with additions of copper selenate and hydrofluosilicic acid were acceptable for both UN in  $UO_2$  and  $UN_2$  in  $UO_2$  prepared samples.

Existing routine methods used in our laboratories gave poor results on both UN and UN<sub>2</sub> content in UO<sub>2</sub> prepared samples. One method consisted of sample digestion in concentrated HCl, or variations of diluted HCl with additions of zinc metal for generation of active hydrogen. Another method was a sample digestion in  $\text{HClO}_4$  and  $\text{H}_2\text{O}_2$  or  $\text{Na}_2\text{O}_2$ .

#### Apparatus and Reagents

Kjeldahl equipment, conventional laboratory glassware, and reagent grade chemicals were used unless otherwise stated.

A NaOH solution was made by dissolving 680 grams of NaOH in two liters of distilled water. Devarda's alloy, 0.5 grams, was added. Solutions were boiled until the volume was reduced to 1.8 liters (9). A mixed indicator of brom cresol green (6) and methyl red was used. Methyl red indicator was used to increase the sensitivity of the end point detection.

#### Procedure

Weigh out about 100 mg. of -100 mesh UO<sub>2</sub> sample into a 50 ml. beaker. Record actual weight. Then add 25 ml. of 1:1 HCl and 1 ml. of H<sub>2</sub>SiF<sub>6</sub>. Do not cover with a watch glass, but heat just below boiling for about 30 minutes. Add about 200 mg. of copper or potassium selenate. Digest until solution is complete.

Transfer the cooled sample solution to distillation Kjeldahl equipment and add 25 ml. NaOH solution. Start distillation to collect the condensate in a 50 ml. Erlenmeyer flask that contains the mixed indicator solution within the 5 ml. of 4% boric acid solution (6). Adjust the heat input so that 5 minutes after distillation begins, about 20 ml. of condensate will be collected. The boric acid solution need not be accurately measured (9).

Titrate the collected ammonia (ammonium borate) with a standard acid of 0.005 normality ( $\underline{N}$ ). Make a blank determination using the same amount of reagent as in the sample determination.

Calculate nitrogen content by the following formula:

Parts per million (ppm) N (nitrogen) = (ml Titration - ml Blank) x N x 14.007 x 1000 Grams Sample

Duplicate results should agree within 0.3% relative.

#### Results and Discussion

The preliminary work as performed on two samples consisting of UN in  $\mathrm{UO}_2$  and  $\mathrm{UN}_2$  in  $\mathrm{UO}_2$ . The results in Table 1 show that several digestion techniques are available or used for analyzing nitrogen as uranium nitrides in  $\mathrm{UO}_2$ . Only the

recommedaded technique, however, gave complete recovery of the nitrogen. An important feature of this digestion technique is the action of the selenate ion. Lathouse et al $(\frac{5}{2})$  showed the selenate ion is essential to the digestion process.

Past efforts to correlate nitrogen values as obtained by vacuum extraction and Kjeldahl techniques were not successful on either commercial samples or prepared samples (Table 1) containing known amounts of UN and UN $_2$  in UO $_2$ .

An analysis of results indicated that the analytical techniques used were biased to particular species of uranium nitride. Some digestion procedures using Kjeldahl techniques gave good values for fused UO<sub>2</sub> containing UN, but were erratic on UN<sub>2</sub> levels in UO<sub>2</sub>. In contrast, the vacuum extraction technique at 1000°C gave good results for UN<sub>2</sub> (U<sub>2</sub>N<sub>3</sub>), but low results for UN in UO<sub>2</sub>. These results seem reasonable since generally reported values show UN is stable in vacuum to about 1700°C.

Vacuum extraction techniques, of course, remain quite useful for measurements of UO<sub>2</sub> sorbed gases that are released at the generally used 1000°C operating temperature. But for fused UO<sub>2</sub> that contains UN or other high temperature stable compounds, a new high vacuum, high temperature technique is needed.

We have modified high temperature vacuum fusion equipment to permit operating temperatures to 2000°C. Present equipment uses a graphite crucible and graphite heat shield. For UO<sub>2</sub>, this graphite reacts at 2000°C with the oxygen in the UO<sub>2</sub> compound to yield copious amounts of CO. This reaction may be useful as an analytical technique for the determination of oxygen-to-uranium atomic ratios in UO<sub>2</sub>. Use of a tungsten crucible and tungsten powder for a heat shield in our vacuum fusion equipment appears to be a promising analytical technique for high temperature compounds such as UN in UO<sub>2</sub>.

#### Removal of Impurities

An important adjunct to these studies showed that high nitrogen levels in fused UO<sub>2</sub> can be reduced to acceptable levels by heat treating UO<sub>2</sub> bulk materials at 1750°C in moist hydrogen.

Fused  $UO_2$  samples originally containing UN and UN<sub>2</sub> were examined after heat treating at 1750°C for 12 hours in moist (1000 ppm  $H_2O$ ) hydrogen. Metallographic examination and nitrogen analysis by the new digestion technique showed depletion of about 80% of the nitrogen content (Table II). Uranium nitrides (UN,  $U_2N_3$ ,  $UN_2$ ) can thus be substantially removed by this process.

#### Conclusions

Generally used digestion techniques for Kjeldahl analysis, and vacuum extraction techniques for analysis of all uranium nitride species present in fused UO2, were inadequate. A satisfactory technique was, however, developed and successfully used.

From our studies on the ease of formation of uranium nitrides in fused  ${\rm UO}_2$ , the writers conclude that uranium nitride formations may also occur in  ${\rm UO}_2$  powders and pellets that are sintered in cracked ammonia. Use of pure hydrogen rather than cracked ammonia in  ${\rm UO}_2$  sintering processes is recommended.

#### Acknowledgement

The authors thank both Mrs. I. S. Parent and Mrs. A. D. Couch for performing many analytical determinations. Thanks are also due to D. W. Brite, and D. R. de Halas and W. E. Roake for their helpful criticisms and suggestions.

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- (3) Cadwell, J. J. "Quarterly Progress Report", Fuels Development Operation, HW-72346 October, November, December, 1961 (Classified)
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- (5) Lathouse, Joan, Huber, F. E. Jr., Chase, B. L. Analytical Chemistry, Vol. 31, December 9, 1959, page 1606-7
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TABLE I. Analysis of Nitrogen as Uranium Nitrides in Fused  ${\rm UO}_2$ 

| Nitrogen (ppm)                         |     |      |            |     |             |
|--|-----|------|------------|-----|-------------|
| Sample                                 | 1_  | 2    | <u>3</u> b | 14  | Theoretical |
| UN (in UO <sub>2</sub> )               | 690 | 890  | 1310       | 250 | 1340        |
| UN <sub>2</sub> (in UO <sub>2</sub> )ª | 540 | 1450 | 1220       | 690 | 1250        |

## Digestion Methods (Kjeldahl Techniques)

- 1. Hydrochloric Acid
- 2. Perchloric Acid and Hydrogen Peroxide
- 3. 1:1 HCl with additions of (copper) selenate and hydrofluosilicic acid.
- 4. Vacuum Extraction at 1000°C with mass spectrometric analysis of gases.
- Some U2N3 possible in sample
- b New Digestion Technique

TABLE II. Removal of Nitrogen as Uranium Nitrides in Fused UO2

# Nitrogen (ppm)

| Sample                                | Before | After (H2 Treatment)        |                          |  |
|---------------------------------------|--------|-----------------------------|--------------------------|--|
|                                       |        | <u>Kjeldahl<sup>a</sup></u> | Vacuum Extraction 1000°C |  |
| UN (in UO <sub>2</sub> )              | 1310   | 265                         | 260                      |  |
| UN <sub>2</sub> (in UO <sub>2</sub> ) | 1220   | 230                         | 388                      |  |

 $<sup>\</sup>frac{a}{}$  New Digestion Technique

# DON'T SAY IT --- Write It!

to Keith Sharp

ROM G. Jansen

I have investigated the references mentioned in the letter concerning the invertion report HWIR—. These reports deal with the treatment of UD, in wet atmospheres to produce sintered and stoichiosom UD. No mention of other impurities vis made atthough the treatments described are nearly idential to those in the invention report. Recent telephore discussions with Wm. De Hollander with GE at San Jose have indicated that wet hydrogen at 1000°C has been successful in removing fluoride from relatively large UD, pellets, the per a probable application to chlorides also. The references investigated are listed on the reverse side of this sheet.

TO MAKE LIFE LAST, PUT SAFETY FIRST

Dehavior of UOz, Webster, A.H. and N.F.H. Bright 2-5-58. Atmosphers:

the N2+Hz, Ar, wet Ar, Ar+Oz, Nz, wet Nz, Nz+Oz, steam at 1200-1500°2.

The effects of atmosphere and stoichionetry on UOz densification were studied.

NP-8393 Sintering of Non-Stoichionetric UOz in different atmospheres.

Nockdstrom, B. and U. Runtors. Studied 90 ratios and densities at 1100-15.

In argon, Hz-Ho atmosphere.

3) J. Amer. Ceramics Soc. 41:179-83(1958) CA Arenberga J.P. Jahn

varied turnere atmosphere, sintering aids, scarling time, furnare atmosphere

PRITISH PATENT & 44980. Not listed in Chem. Abstracts.

I have sent for a copy of the patent.

August 3, 1962

U. S. Atomic Energy Consission Chicago Operations Office 9800 South Case Avenue Argonno, Illinois

Attention: Mr. George H. Lee, Chief

Chicago Patent Group

#### Gentlemen:

Enclosed berevith are three copies of an invention report, General Electric Case B(IS-15)3, extitled 'A Nothed to Furify Muclear Grade Uranius Dioxide ( $\mathbf{UO}_2$ ) Grain', subsitted by H. J. Anderson, R. J. Anterson, B. J. Anterson,

The hydrogen tractions of UO, to edjust the O/U ratio has, I understend, been known previously. The point of novelty in the present case is the use of the <u>point</u> hydrogen. While the limits of water content have not been accurately determined as yet, the order of engaltude appears to be important. If the amount is too low, the important are not effectively recoved. If it is too high, the O/U ratio is increased.

I understand that what I consider the invention originated by socident. It was observed that an improvement in results had occurred at a time when an assistant had allowed the dehydrating agent treating the hydrogen to become exhausted. The inventors hope to investigate the satter of water concentration in more detail.

References 1-4 are classified.

Two copies of MF-5A-R66; - Determination and Control of Mitrogen as Ursains Mitrides in Pused Ursains Dioxide (UG<sub>0</sub>) are enclosed and clearance is requested for publication in SMADTICAL CHRISTON. If

clearence cannot be given promptly (by shout Deptember 1, 1962), we would appreciate being informed. The authors would then delete all pessenges disclosing the subject anther of this invention, thus limiting the paper to the determination of mitrogen.

While the invention is useful in commection with the Pick, it apparently did not arise specifically under the Plutonius Recycle Program. I have not sent the disclosure to Mr. Robertson.

Very truly yours,

Robert Keith Mary Patent Athornay

RED: OR

Mclomres

en: UBAEC-NOC - Att n: Production Division

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HWIR-1533 LB Awarting Cleanance - L13.

# DETERMINATION AND CONTROL OF NITROGEN AS URANIUM NITRIDES IN FUSED URANIUM DIOXIDE (UO2)

By Harlar J. Anderson and James C. Langford

Hanford Atomic Products Operation General Electric Company Richland, Washington\*

#### Introduction

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In our laboratories, vacuum extraction and Kjeldahl techniques are used to analyze for fixed or sorbed gas content in UO<sub>2</sub> samples. Past efforts to correlate nitrogen values obtained by these two analytical techniques with calculated values of prepared samples containing known amounts of UN and UN<sub>2</sub> in UO<sub>2</sub> have not been successful. Nitrogen values for samples of commercial fused UO<sub>2</sub> supplies have also not been in agreement between vendor and our laboratories. Because of this inconsistency among analyses, study of these analytical techniques was under taken and completed.

A new analytical technique was developed and successfully used to analyze the nitrogen content (UN,  $U_2N_3$ ,  $UN_2$ ) in fused  $UO_2$ .

<sup>\*</sup> Work performed for the U.S. Atomic Energy Commission under Contract AT (45 1) 1350.

#### Abstract

A new Kjeldahl digestion technique that uses a mixture of 1:1 diluted hydrochloric acid with additions of copper selenate and hydrofluosilicic acid was successfully used to analyze the nitrogen content (UN,  $U_2N_3$ ,  $UN_2$ ) in fused uranium dioxide ( $UO_2$ ). Generally used digestion techniques and vacuum extraction at  $1000^{\circ}$ C are inadequate for analysis of all uranium nitride species present in (fused)  $UO_2$ . An important adjunct to these studies showed that high nitrogen levels in  $UO_2$  can be reduced to acceptable levels by heat treating bulk  $UO_2$  supplies at  $1750^{\circ}$ C in moist hydrogen.

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Reagents that might be effective in dissolving  $UO_2$  have been reported (2). Determination of nitrogen in  $UO_2$  has been reported (7) by Bennett using a method of oxidizing alkaline fusion followed by measurement of the volume of released nitrogen. Generally, the analytical approach for nitrogen determination was the Kjeldahl method with modifications of digestion techniques (8). A note (5) on a method for the determination of nitrogen content in uranium nitrides was important since these nitrogen species were identified as present in our fused  $UO_2$  supplies.

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From our studies on the ease of formation of uranium nitrides in fused  ${\rm UO}_2$ , the writers conclude that uranium nitride formations may also occur in  ${\rm UO}_2$  powders and pellets that are sintered in cracked ammonia. Use of pure hydrogen rather than cracked ammonia in  ${\rm UO}_2$  sintering processes is recommended.

#### Acknowledgement

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TABLE I. Analysis of Nitrogen as Uranium Nitrides in Fused UO2

| Nitrogen (ppm)                                 |     |      |            |     |             |
|--|-----|------|------------|-----|-------------|
| Sample   |     | 2    | <u>3</u> b | 14  | Theoretical |
| UN (in UO <sub>2</sub> )                       | 690 | 890  | 1310       | 250 | 1340        |
| UN <sub>2</sub> (in UO <sub>2</sub> ) <u>a</u> | 540 | 1450 | 1220       | 690 | 1250        |

## Digestion Methods (Kjeldahl Techniques)

- 1. Hydrochloric Acid
- 2. Perchloric Acid and Hydrogen Peroxide
- 3. 1:1 HCl with additions of (copper) selenate and hydrofluosilicic acid.
- 4. Vacuum Extraction at 1000°C with mass spectrometric analysis of gases.
- a Some U2N3 possible in sample
- $\underline{b}$  New Digestion Technique

TABLE II. Removal of Nitrogen as Uranium Nitrides in Fused  ${\rm UO}_2$ 

# Nitrogen (ppm)

| Sample                                | Before | After (H2 Treatment)        |                   |        |
|---------------------------------------|--------|-----------------------------|-------------------|--------|
|                                       |        | <u>Kjeldahl<sup>a</sup></u> | Vacuum Extraction | 1000°C |
| UN (in UO <sub>2</sub> )              | 1310   | 265                         | 260               |        |
| UN <sub>2</sub> (in UO <sub>2</sub> ) | 1550   | 230                         | 388               |        |

 $<sup>\</sup>frac{a}{}$  New Digestion Technique

# PATENT SPECIFICATION

NO DRAWINGS

844,980



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Complete Specification Published August 17, 1960.

Index at Acceptance: Class 1(3), AlN36. International Classification: Colg

# Method of producing dense uranium oxide bodies.

#### COMPLETE SPECIFICATION

We, UNITED STATES ATOMIC ENERGY COMMISSION, 1901 Constitution Avenue, Washington, District of Columbia, United States
of America, an agency of the United States
Government established by the Atomic
Energy Act of 1946 (Public Law 585) and
the Atomic Energy Act of 1954 (Public Law
703), do hereby declare the invention for
which we pray that a patent may be granted
to us and the method by which it is to be
performed, to be particularly described in
and by the following statement:

This invention relates to the production of dense uranium oxide bodies that are particu15 larly suitable for use as fuel elements in

atomic reactors or furnaces.

In the operation of such reactors considerable heat is generated from the fuel elements and is customarily dissipated by water cool-20 ing. At the elevated temperature involved. however, water vapor or steam has a strong tendency to corrode and disintegrate such fuel elements which must therefore be designed to withstand these effects. Inasmuch 25 as porous bodies are more easily penetrated, and hence more subject to such deteriorating influences, high density, and consequently low porosity, is highly desirable from this standpoint. Accordingly, the minimum ac-30 tual density of uranium oxide elements, as compared to the theoretical density of the material, should be about 90%, and a density ratio of 95% or higher is commonly specified.

A further factor in the design of atomic fuel elements is capacity to retain fission pases generated within the fuel elements during operation of the reactor. There is evidence to indicate that the capacity of a 40 fuel element to retain such gases increases with its density and astronomy designs beginning.

with its density, and extremely dense bodies are desirable for this reason as well.

Heretofore uranium oxide fuel elements have been molded in pellet form and such pellets densified by sintering in a hydrogen

atmosphere at a temperature of about 1750° C. for a period of time up to 10 hours. This consumes a considerable amount of hydrogen, a relatively expensive material. Furthermore, the attainment of such temperatures generally requires special furnaces constructed with molybdenum or tungsten heating elements. Such furnaces are expensive to construct, and limited as to firing capacity. Also, they must be operated in a special nonreactive atmosphere such as hydrogen, helium, or argon to protect the heating elements. As a result the hydrogen firing operation, while quite effective for the purpose, is extremely expensive.

It is then a primary purpose of the present invention to meet the need for a more economical method of sintering uranium oxide bodies to a high density. It is a further purpose to provide such a sintering method capable of being carried out at lower temperatures, for example about 1300°C., attainable in a conventional type furnace, such as a muffle furnace with silicon carbide type resistance heating elements. Another purpose is to minimize the use of hydrogen and substitute a less expensive sintering atmosphere.

These ends may be achieved by practising our present invention which consists in a method of producing a dense uranium oxide body which comprises sintering in a steam atmosphere a body of uranium oxide grains having an oxygen-uranium atomic ratio not over 2.04, said grains having a particle size of less than 1 micron average diameter. Preferably said ratio is less than 2.02 and the sintering temperature is 1300°—

1400°C.

Uranium oxide, in its reduced state, or lowest state of oxidation, theoretically contains oxygen and uranium atoms in a ratio of 2 to 1, as indicated by the formula UO<sub>1</sub>. It readily takes up additional oxygen however, and commercially available material usually has a somewhat higher ratio.

(Price 3s. 6d.)

PAOPER

Before such commercial material is molded and fired into fuel elements or other bodies, it is granulated to impart proper molding properties. In this operation the 5 uranium oxide is mixed with liquids, binders, and lubricants to form a wetted mass suitable for conversion into granules having a range of particle sizes particularly suitable for molding a uniform body.

If the uranium oxide contains coarse grains or large aggregates, it is necessary to break these up so that the ultimate grains are smaller than one micron average diameter. It is customary to ballmill the urani-15 um oxide to achieve this desired size reduction and/or deagglomeration; however, other physical or chemical methods which achieve the same result are equally suitable.

We have now found that, during the cus-20 tomary ballmilling operation, the ratio of oxygen to uranium atoms (hereafter referred to as O/U ratio) increases to a value of 2.10 to 2.20 depending on the length of time involved. We have further found that this 25 change in the O/U ratio substantially interferes with sintering of this material in steam in accordance with the present invention, thus defeating the purposes of the invention. The manner in which the extra oxygen atoms 30 are held is not definitely known. However powder X-ray diffraction analyses indicate that no new crystal structure is involved. but rather that a type of chemisorption occurs with the oxygen being held along crys-35 tallite boundaries and apparently producing fractures in, and consequent reduction in size of, the crystallites,

In any event, it is essential for present purposes that excess oxygen be removed so 40 that the uranium oxide, prior to steam sintering, has an O/U ratio of 2.04 or less. While material with a ratio up to 2.04 can be sintered to a relatively dense body, optimum densities require a ratio under 2.02 45 and such lower ratio is preferred.

Reduction is conveniently accomplished by a hydrogen firing step prior to steam sintering. We have found that satisfactory results can be obtained by firing uranium ox-50 ide bodies in a hydrogen atmosphere for a period of about two hours at about 1200°C. just prior to the steam sintering step. At

higher temperatures sintering is initiated to such an extent that the resulting crystallites do not respond in the desired manner to the 55 steam sintering process.

The bodies may also be brought to a temperature of about 1200°C. in a hydrogen atmosphere, but this is unnecessary and uneconomical since equally good results can be 60 obtained with other types of firing atmospheres in this initial heating period. While a steam atmosphere may be used in this initial heating, it is generally desirable to employ a neutral or reducing atmosphere such as 65 nitrogen or cracked ammonia, providing such materials are readily available.

In a typical firing operation, shaped bodies are introduced into a cold furnace and a flow of gas, such as nitrogen, or steam, started in the furnace or firing muffle and maintained while the temperature is raised to about 1200°C. The furnace is held at that temperature for two hours with a flow of hydrogen replacing nitrogen. At the end of this 75 time the hydrogen atmosphere is replaced with a steam atmosphere and the temperature raised to about 1300°C. and maintained at this temperature for about four hours.

While it is generally more convenient to 80 perform the reduction just prior to steam sintering and then sinter in situ, this is not essential. Thus the reduction may even be performed prior to granulating and pressing or at any intermediate stage, providing the material is maintained at the desired low O/U ratio up to the time of steam sintering.

Surprisingly enough we have found that the O/U ratio increases during the course of such steam firing to about 2.19. In view 90 of this circumstance it seems rather anomalous to reduce the ratio in the ballmilled material prior to steam sintering. However, repeated experiments have confirmed that such reduction is a prerequisite to effective 95 steam sintering.

The actual sintering temperature required for a particular purpose will depend on the material density desired and will also vary with time of sintering. The following table 100 indicates densities obtained with graduated sintering times and temperatures, and will serve as a guide in practising the invention.

| 105 | Temperature in *C.<br>1200<br>1300<br>1300 | Time in hrs. 8 1 2 | Density in gm/cc<br>10.39<br>10.06<br>10.32 | Density in %<br>94.8<br>91.8<br>94.2 |
|-----|--|--------------------|---|--------------------------------------|
| 110 | 1300<br>1400<br>1400<br>1500               | 1<br>2<br>2        | 10.60<br>10.48<br>10.57<br>10.60            | 96.7<br>95.6<br>96.4<br>96.7         |
| •   |  | KUMEMIY            |   |                                      |

The data in the last column represent the percentage ratios of the actual densities in the preceding column to a theoretical density

of 10.96 gm/cc.

5 Below 1200°C, sintering occurs so slowly, it at all, as to be negligible. Even the 8 hour time at 1200°C, is generally too long to be practical. On the other hand it is difficult to attain temperatures over 1400°C, without special firing furnaces involving heating elements sensitive to oxidation. For these reasons it is generally preferable to employ a sintering temperature of 1300-1400°C.

We have further found that the nature of the sintered material is dependent on the post-sintering or cooling treatment. If the sintered body is cooled in a steam atmosphere, X-ray diffraction tests indicate that the resulting mixed crystal structure is composed of two cubic phase crystals, UO<sub>1</sub> and UO<sub>2-25</sub>, in the ratio of approximately 1:3. However, if the steam atmosphere is re-

placed at the completion of sintering and the sintered material cooled in a reducing at-25 mosphere such as hydrogen, a single cubic phase crystal structure having the diffraction pattern of UO<sub>2</sub> and having an O/U ratio of 2.03 or less is obtained.

WHAT WE CLAIM IS:-

A method of producing a dense uranium oxide body which comprises sintering in a steam atmosphere a body of uranium oxide grains having an oxygen-uranium atomic ratio not over 2.04, said grains having a particle size of less than 1 micron average diameter.

2. The method set forth in claim 1 in which the oxygen-uranium atomic ratio is less than 2.02.

40 3. The method set forth in claim 1 in

which the sintering temperature is 1300—1400°C.

4. The method set forth in claim 1 in which the body is fired at a temperature of 1200°C. for a period of about two hours in a hydrogen atmosphere to reduce the ratio of oxygen and uranium atoms to a value not greater than 2.04 prior to steam sintering.

5. The method set forth in claim 1 in which the uranium oxide from which the 50 body is produced is initially subjected to a size reduction operation in which the oxygen-uranium ratio is increased and, prior to the sintering step, the ratio is reduced to a value not exceeding 2.04.

6. The method set forth in claim 1 in which the sintered product is cooled in a

steam atmosphere.

7. The method set forth in claim 1 in which the sintered product is cooled in a hy- 60

drogen atmosphere.

8. The method of sintering a molded body of uranium oxide which comprises bringing the body to a temperature of at least 1200°C. with an oxygen-uranium ratio, 65 on an atomic basis of not over 2.04, and introducing and maintaining a steam atmosphere over the body while it is held at the sintering temperature,

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