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BIOPHYSICS SECTION RADIOLOGICAL SCIENCES DEPARTMENT

INTERIM REPORT ON THE RADIOCHEMICAL ANALYSIS OF HANFORD REACTOR **EFFLUENT WATER**



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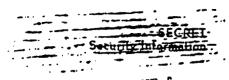
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INTEL A REPORT ON THE RADIOCHEM ANALYSIS OF HANFORD REACTOR EFFLUENT WATER

April 20, 1953

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R. L. Watters E. E. Larkin

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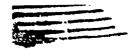
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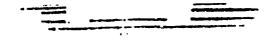
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INTERIM REPORT ON THE FADIOCHEMICAL ANALYSIS OF HANDORD REACTOR EFFICIENT WATER

INTRODUCTION:

The Biophysics Control Laboratory, Fadiological Sciences Department, has studied and analyzed reactor effluent water for the various beta particle emitting isotopes on a routine basis since late 1950. The objectives of this work were the identification of the radioactive isotopes present and the recognition and explanation, if possible, of any trends in the isotope spectrum throughout the year.

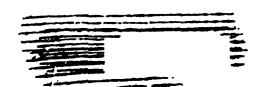
An earlier report (1) contains the routine sampling and analytical procedures with the presentation of earlier results. The present report gives a discussion of new isotopes found, corrections made in counting factors, and a detailed discussion of results obtained during the period from January, 1951, to June, 1952.

SUMMARY:

Several fission products have been identified and quantitatively determined in reactor effluent water. From the attivity densities determined, an estimation of the uranium available for releasing fission products to the cooling water has been made assuming instantaneous release of the fission products to the water. The analytical data obtained indicate that approximately 85% of the total beta particle emitting isotopes have now been properly identified. Certain variations of total beta particle activity and isotopic spectrum between reactors and during different seasons are noted, but lack of sufficient data prevents actual definitions and correlations. Revised procedures for sodium and the rare earth elements are included in the appendix with those procedures adopted for the determination of iodine, strontium, and barrum.

PROCEDURES:

The isotopes of atmostrum and barrum were apparated from the effluent water initially by precipitation of the lambonates in the presence of partier. This pre-







cipitate was dissolved and the strontium and barium separated from calcium by precipitation of strontium and barium nitrates in fuming nitric acid. The barium and strontium were finally precipitated as the chromate and oxalate, respectively.

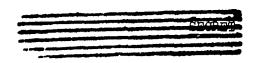
Decay curve analysis was used to identify the two isotopes Sr⁹¹ and Ba¹³⁹.

Separation of the total iodine isotopes was accomplished by a distillation method in which the iodide was oxidized to free iodine with nitrous acid and (3) collected in carbon tetrachloride. The iodine was reduced with sodium bisulfite, extracted into water and precipitated as palladous iodide. The decay curve of the total 2 dine isotopes was then analyzed to determine the amount of I¹³¹ present.

The analytical procedure for the rare earth isotopes (1) was revised to eliminate the zirconium iodate step and the consequent loss of part of the rare earth fraction to the iodate precipitate. This change was possible because the zirconium present was effectively removed in the fluoride precipitation and the low thorium concentrations did not significantly affect the rare earth determinations. This revision of procedure resulted in a significant increase in the rare earth concentrations reported.

The analytical procedure for sodium reported previously (1) has been shortened by limiting scavenging steps to one sulfide precipitation from an ammoniacal solution. A calcium oxalate precipitation could probably be made at the same time but this step has been carried out separately as a qualitative check on the activity from the alkaline earths.

Backscatter measurements were made by mounting the isotope on formvar film, which had previously been found to give negligible backscatter (4), and measuring the counting rate with and without stainless steel backing. The ratio of the counting rate with the stainless steel backing to that with formvar backing only, gave the backscatter correction factor.





The effluent analysis data were compiled for the period from January, 1951, to June, 1952, and a statistical study tarried out. These data were analyzed for variation of total beta activity density and of the isotopic spectrum with different reactors and different seasons of the year. All data were adjusted for variations in power level and flow rate of cooling water before correlations were attempted by assuming linear relationship between activity and power level and by comparing activity per unit time rather than activity density. The significance of the differences existing in effluents was determined by I-test.

RESULTS:

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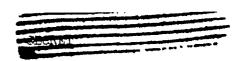
Six individual isotopes, as well as the rare earth group, all of which can be formed from fission, have been identified. The activity density of the effluent contributed by each of these isotopes is given in Table I along with similar figures for those isotopes formed by (n, y) reaction. Measurements on individual samples are included in Table III. The summation of average contributions by the isotopes accounts for approximately eighty-five percent of the total beta activity.

TABLE I
BETA PARTICLE EMITTERS IN REACTOR WASTE EFFLUENT

Isotopes Formed	Average		Isotopes	Average	
By (n, γ)	Activity Density	Ave.	From	Activity Density	Ave.
Reaction	Units of 10-6 ue/ca	76	Fission	Units of 10°6 uc/cc	<u></u>
a. Ch	537	077	R.E Y(2)	3.00	6.5
Cu - 64	537	27			
Mn - 56	450	22	R.E. + Y	68	3•3
Na - 24	302	15	Ba - 139(1)	29	1.6
Si - 31	175	7.3	Sr - 91	12	0.67
As - 70 (2)	50	2.2	Mo - 99	3•3	0.20
1 (total)(1)	27	1.4	I - 131	0.33	0.014
Cr - 51	9.4	0.51	Ba - 140	0.37	0.020
P - 32	9.0	6.39	S zr - 89	0.12	0.0039
Fe - 59		0.01			
Ca - 41, 45, 47	< 1.1	< ೧.05			

- (1) This figure includes activity from both fission and (n, y) reaction.
- (2) Results of analysis for rare earth-yttrium fraction by revised procedure.
- (3) Results of analysis for rare earth-yttmium fraction by original procedure(1).





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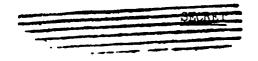
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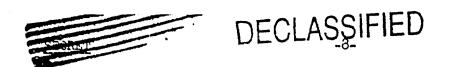
It was found that there were no significant differences between Areas in the activity density measurements in 1951 but that the activity density of reactor effluent in 100-H Area was significantly lower than that in all other areas during the period in 1952. With the exception of 100-H Area, the measurements made in 1952 were significantly higher in all areas than they were during the same period of 1952. The increase could not be accounted for by increased power levels if the linear relationship is assumed. Some evidence of higher concentrations of total beta particle emitters in reactor effluent water during the spring season were noted during 1951, but it was neither pronounced nor definite. The marked increase of such measurements in 1952 may well be due to more pronounced effect of the possible seasonal variation.

During the period from January, 1951, to October, 1951, when water treatments in all areas were similar with use of ferric sulfate as coagulant, the only highly significant difference for those isotopes measured occurred in the presence of higher concentrations of Mn⁵⁶ in the reactor effluent water at 100-DR than those in the effluent from other areas. This may possibly be explained by the limited chlorination of the water in this area before the coagulation step.

After October, 1951, when aluminum sulfate was substituted for ferric sulfate as the coagulating agent at 100-F, significantly lower concentrations of Cu⁶⁴ were observed in the reactor effluent water from that area. These lower concentrations were significantly different from previous values at 100-F and from concentrations in other areas during the same period.

Two further changes, the addition of silica as a coagulating agent at 100-F after January, 1952, and the omission of the sodium dichromate after April, 1952, at all areas cannot be fully evaluated from this data. Marked increases were noted during the early months of 1952 in the Mn⁵⁶ content of the water at 100-F. This increased concentration, significantly different from that at all other areas, may





be due to the presence of manganese in the lime which was added after the coagulation step in the water treatment at 100-F.

Concentrations of Si³¹ were higher in effluents from all areas during 1952 than during the same period in 1951 and the concentrations of this isotope in effluent from 100-B were significantly higher than in effluent from all other areas during 1952. Concentrations of As⁷⁶ were higher in the effluents from all areas except 100-DR during 1952. Concentrations of Mn⁵⁶ continued to be significantly higher at 100-DR than from all other areas except 100-F.

Counting corrections for certain isotopes have been revised and are given in Table III. All other factors are those used in previous calculations (1). These factors apply for measurements using the conventional mica-window counter.

TABLE III
REVISED COUNTER CORRECTIONS

•	Window and Air	Backscatter
Isotope	Absorption Correction Factor	Factor
Mn 50 Cu 64	1.05	1.04 *
Qu ^{O4}	1.2	1.2
R.E. + Y Cr ⁵¹	1.3	1.3
Shelf 1	1.5	
2	1.9	
3	2.0	

- * Mounted on filter paper. All other isotopes are mounted on stainless steel, 0.006" thick.
- 1 Recent measurements by the Radiochemical Standards forces of Radiological Sciences have indicated that the backscatter factor for ${\rm Cu}^{64}$ may be as much as 1.4 resulting in more conservative figures for ${\rm Cu}^{64}$.

Earlier work has shown Ba¹⁴⁰, a fission product, to be present in reactor effluent water under normal operation conditions⁽¹⁾. However, concentrations were not accurately determined. Further work initiated in this group for the development of reliable analyses for fission product in the reactor cooling water after a slug rupture revealed that concentrations of I¹³¹ in normal reactor cooling water were of the same order of magnitude as those of Ba¹⁴⁰ (5). This led to an intensive



search for fission products in the cooling water during normal operation.

Two other isotopes with possible fission source that have been identified and determined quantitatively are Ba and Sr lead of the latter is apparently in a mixture of all the strontium isotopes which would be present four hours after release from the reactor and is the predominant isotope measured by the counting methods used. It should be noted that the Ba concentration may not all be produced by fission since this isotope may be formed from Ba lead of the neutron-gamma reaction. Indications of tellurium and zirconium isotopes have also been found but quantitative values await the development of specific and efficient separations.

The rare earth fraction is of special interest since it is possible that the bulk of this activity could come from fission isotopes. A comparison of the decay curve of this fraction with the decay curve of the rare earths formed by fission indicates that this is quite possible.

Calculations have been made to determine the uranium in the reactor available for release of fission products to the effluent water assuming immediate release of fission products to the water. The results of such calculations are shown in Table IV and are based on the assumption that the flow rate of reactor effluent was 130,000 liters/minute with neutron flux equal to 10^{13} n/cm²/sec. These results indicate that some or all of the fission products may be retained in the film on tubes and slugs for an undetermined length of time.

TABLE IV
URANIUM NECESSARY FOR FISSION PRODUCTS IN REACTOR EFFLUENT

Isotope Used	Isotopic Activity in Effluent Leaving Reactor Units of 10-6 uc/cc	Conc. U
Ba ¹³⁹ Ba ¹⁴⁰ Sr ⁸⁹ Sr ⁹¹ ₁ 131	240 0.50 0.077 9.9 0.77	19 10 6.4 3.6 20





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Possible sources of this wranium may be the natural wranium in the cooling water, wranium present on the outside of the slugs when 'bey are inserted into the reactor, and that wranium possibly left in the tubes from previously ruptured slugs. Measurements in cooling water entering the reactor at 100-B indicate natural wranium concentrations in the cooling water equal to 0.25 ug/liter. This wranium in the cooling water may be a source of wranium in the film. Complete surface smears made on slugs just before they entered the reactor at 100-F on November 23, 1951, showed an average amount of wranium per slug removed by this means to be 7 ug with as much as 40 ug of wranium being removed from one slug. The order of magnitude of that wranium contributed by the third means has not been measured.

Further work will be carried out to determine the effect of seasonal changes on the effluent as well as the effect of changes in water treatment prescribed by the Water Quality Studies Group of the Technical Section, Engineering Department.

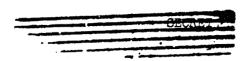
ACKNOWLEDGEMENTS:

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personnel who collected the samples analyzed, and the Radiological Sciences Control

Services personnel who carried out the statistical studies.





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Sample Location	100-B	100~B	100-B	100-B	100-B	100-B
Sampling Date	2-15-51	2-23-51	3-13-51	3-20-51	14-6-51	6-12-51
Sampling Time	0460	0660	0660	0060	0480	0350
Total Beta Activity Density, units of 10-3 uc/cc	1.7	1.6	1.9	2.6	1.4	1.9
% Total Bets Activity						
Manganese ~ 56		•	17	23	ı	25
Sodium - 24	ı	13	ส	52	ı	27
Copper - 64	ı	58	33	19	t	50
Arsenic - 76	•	1.3	3.5	1.5	•	1.3
Rare Ex:ths + Y	5•3	ı	1	8.4	3.2	1
Silicon - 31	ı	•	ı	1	•	ı
Phosphorus - 32	ı	ı	0.19	99.0	•	64.0





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EC V	TABLE V (Cont.) ACTIVITY OF MAJOR CONSTITUENTS OF REACTOR EFFLUENT WATER	AA.TOR CONS	TABLE V (Cont.)	(Cont.) OF REACT	R EFFLUEN	T WATER		
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1000 T of cont.	100-B	100-B	100-B	100-B	100-B	100-B	100-B	T00T
Sample bock of the			בא בת מ	0-11-51	9-54-51	10-30-51	10-30-51 11-15-51 12-5-51	12-5-51
Sampling Date	6-27-51	TC-4Z-).	エイーターの	-/				
Sampling mine	0660	0060	0915	0260	1005	0955	0930	0350
rotal Beta Activity Density, units of	1.9	1.7	.3	2.1	2	2.0	£• 1	1.9
% Total Beta Activity							·	ç
, ,	6	31	19	15	15	17	0.	4
Manganese - 70	3	ξ :	, α	71	13	ខ្ព	6.2	17
Sodium - 24	य	य	0	-	} '	(ŭ	70
Comer • 64	%	34	23	35	26	53	6	ī -
o toddoo	3.0	1,0	1.0	0.5	6.0	7.0	†• 0	4
Arsenic - (0	ì		,	•	•	1	1	* †1
Rare Earths + Y	•	•	•			œ:	0.5	5.5
[6]	4.9	5.8	7.0	8.2	5.8	•	1.0	
	20	0.0	ı	•	0.22	0.78	•	8 ⁴ .0
Phosphorus - 32	20.0) •						

* Results obtained by revised method of analysis.

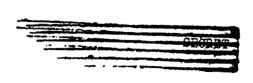
Phosphorus - 32





	ACTIVIT	ACTIVITY OF MAJOR CONSTITUENTS OF	R CONSTIT	UENTS OF	REACTOR EFFLUENT WATER	FLUENT W	ATER		
Sampling Location	100-B	100-B	100-B	100-B	100-5	מייטרנ	100 - B	100-B	100 -B
Sampling Date	1-22-52	2-11-5	2-18-52	3-18-52	4-14-52	5-1-5	6-4-52	6-18-52	6-30-52
Sampling Time	0925	0060	0925	0860	0350	00,00	0945	9260	0760
Total Beta Activity Density, units of 10-3 uc/cc	1.9	4.5	7.5	2.8	3.5	5.6	6.5	3.2	7.5
% Total Beta Activity	젊								
Manganese - 56	य	6.5	1,3	25	55	7.1	91		16
Sodium - 24	71	зв	15	12	13	ħ.	75	15	<u>.</u> .
Copper - 64	27	56	28	58	58	34	18	17) 9 1
Arsenic - 76	† • †	3.3	7.1.0	1.5	5.3	3.0	1.5	0.00	•
Rare Earths + Y	•	7.7	۳. ع	5.4	6.3	5.9	5.2	η•6	5.1
Silicon - 31	9•3	7.6	6.3	6.5	7.6	13	21	77	91
rnosphorus - 32	0.77	1.3	0.37	0.58	0.26	0.42	05.0	0.51	0.38







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7	ACTIVITY OF MAJOR CONSTITUENTS	F MAJOR C	TABLE		Cont.) OF REACTOR EFFLUENT WATER	UENT WATE	œ۱		
Sample Location	100-D	α- 00 τ	100-D	100-D	100-0	100-D	100-D	100-D	
Sampling Date	2-27-51	5-6-51	5-10-51	5-18-51	7-3-51	6-1-51	8-28-51	9-17-51	. •
Sampling Time	0660	1100	0160	0350	1000	315	0915	0060	
Total Beta Activity Density, units of 10-3 uc/cc	1.8	ري د	2.3	5.6	1.9	1.6	1.9	۵ ښ	
% Total Beta Activity									
Manganese - 56	20	ಚ	ಜ	20	23	20	15	14	
Sodium - 24	15	7,7	6	13	t	19	91	ជ	
Copper - 64	55	†Z	Ħ	ส	31	04	35	19	
Arsenic - 76	3.0	3.1	3.1	6.0	0.1	6.0	5.6	0.2	
Rare Earths + Y	1	ı	•	1	ı	3.4	ı	•	
Silicon - 31	ı	t	•	9.6	0.6	7.7	9•9	6.1	
Phosphorus - 32	0.37	11.0	1	ŧ	ı	•	1	•	



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Sampling Date	11-13-51	11-26-51	12-11-21	11-13-51 12-11-51 12-51 12-51	2-4-5	2-12-52	3-3-52	4-3-72
Sampling Time	9160	1005	0935	0920	915	0630	9460	0915
Total Beta Activity Density 1.5 units of 10-3 uc/ca	ty 1.5	2•3	2.2	ቱ. ሪ	2.5	2.1	1.8	3.0
% Total Beta Activity								
жилдвлеве - 56	6.9	23	[†] 1	13	01	15	25	16
Solium - 24	13	র	ជ	13	15	13	16	13
copper - 64	775	18	20	32	38	30	715	19
Araenic - 76	9.0	0.3	1	ı	4.1	4.5	1	1.4
Rere Earths + Y	1		•	ı	5.8	4.9	1.0	1.9
Silicon - 3.	3.8	0.9	6.2	5.8	4.7	1.5	9.5	6.2
Phosphorus - 32	9.0	0.28	0.53	0.59	0.42	0.43	Q † *0	0.52



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ACTIVITY OF MAJOR CONSTITUENTS OF REACTOR EFFLUENT WATER	100-1	4-30-52	0925			318	15	53	2.7	4.3	ជ	54.0
AG	Sample Location	Sampling Date	Sampling Time	Total Beta Activity Density units of 10-3 uc/cc	& Total Beta Activity	Manganese - 56	Sodium - 24	Copper - 64	Arsento - 76	Rare Earths + Y	Silicon - 31	Phosphorus - 32



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100-DR

						•	•			~		
	100-DR	5-1-51	0670	2.3	6 ,	18	19	0.4	•		0.03	
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MAJOR CONS	100-DR 7-5-51 0950 2.5	25 12 25 0.22 - 6.3
TABLE V (ACTIVITY OF MAJOR CONSTITUENTS	100-DR 6-4-51 0945 2.3	35 16 27 5.5 -
AC	Sample Location Sampling Date Sampling Time Total Beta Activity Density units of 10-3 uc/cc	Manganese - 56 Sodium - 24 Copper - 64 Arsenic - 76 Rare Earths + Y Silicon - 31 Phosphorus - 32





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		ACTI	VITY OF MA.	JOR CONSTI	ACTIVITY OF MAJOR CONSTITUENTS OF REACTOR EFFLUENT WATER	EACTOR EF	TUENT WATE	æ		
Sample Location	100-DR	100-DR	100-DR	100-DR	100-DR	100-DR	100-DR	100-DR	100-DR	100-DR
Sampling Date	1-2-52	1-30-52	2-25-52	3-4-52	3-13-52	4-1-52	4-29-52	5-19-52	6-2-52	6-23-52
sumpling Time	0830	0460	0860	0915	0915	9060	945	1005	0925	10 i 0
Total Beta Activity Density, units of 10-3 uc/cc	3 2,3	2.0	2.9	3.0	3.0	3.0	2.5	2.4	5. 4. 2.	4.0
\$ Total Beta Activity	147									
Manganese - 56	91	ช	31	50	Τ †	33	₩	83	27	8
Sodium - 24	72	п	10	ជ	7,7	1,4	3.6	97	4.8	ឧ
Copper - 64	30	25	25	23	18	50	19	83	ជ	25
Arsenic - 76	1.3	4.3	3.4	1.0	4.1	0.25	2.1	61.0	₹ - Ħ	92.0
Rare Earths + Y	ı	ı	6.9	8.4	4.5	1. 1	3.2	3.9	3.	5.4
Silicon - 31	9.7	6.3	5.5	4.7	5.1	2.9	9.9	य	01	† T
rhosphorus - 32		0.62	1.3	0.42	0.61	•	o.4€	0.35	0.29	0.32

		ACTIVI	ACTIVITY OF MAJOR CONSTITUENTS OF REACTOR EFFLUENT WATER	OR CONSTIT	TABLE V (Cont.	nt.) REACTOR	EPFLUENT	WATER			
Sample Location	100-F	100-F	100-F	100-F	100-F	100-F	100-F	100-F	100-F	100-F	
Sampling Date	1-2-51	2-14-51	2-20-51	2-28-51	3-12-51	3-27-51	4-2-51	4-9-51	4-18-51	5-14-51	
Sampling Time	9550	1040	0060	0060	0260	0060	9460	0855	1005	1000	
Total Beta Activity Density, units of 10-3 uc/cc	1.4	9.0	1.5	1.9	2.3	2.5	4.5	5.6	1.3	1.9	
f Total Beta Activity	ĸ										
Manganese - 56	₹	•	t	56	54	16	39	25	20	37	
Sodium - 24		1	59	55		14	ซ	54	2	6	
Copper - 64	•	ŧ		56	21	22	20	16	† ₹	01	
Arsenic - 76		ı	•	12	5.6	7.3	3.3	2.7	3.9	4	
Rare Earths + Y		6.2	•	•	1	1.6		3.8	ı	•	
Silicon - 31	:		•	•	ı		•	•	•	•	
Phosphorus - 32	6.0	•	•	0.52	0.33	0°0	0.14	0.24	0.24	0.3	

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		ACTIVITY	OF MAJOR	TABLE	TABLE V (Cont.)	L EACTOR TF	ACTIVITY OF MAJOR CONSTITUENTS OF REACTOR FFFLUENT WATER	Ter		
Sumple Location	100-F	100-	100-	100-F	100-F	100-F	100 -F	100-F	100-F	100-7
Sampling Date	6-20-51	7-17-51	7-19-51	t-15-51	9-4-51)-12-51	10-15-51	10-24-51	10-15-51 10-24-11 11-19-51 12-10-51	12-10-51
Sampling Time	0510	0460	0660	01/0	0,725	0860	1030	07/0	0630	060
Total Beta Activity Density, units of 10-3 uc/cc	€	1.6	2.0	2.2	6.0	1.8	1.6	1.8	1.1	1.8
% Total Beta Activity										
Manganese - 56	17	22	ä	27	50	27	56	5.1	.5	36
Sodium - 24	15	23	15	17	13	•	20	12	13	15
Copper - 64	17	35	य	30	23	31	23	8	80	17
Arsenic - 76	0.3	1.1	7.1	9.0	•	1.1	0.7	1.5	1.0	1.2
Rere Earths + Y				:	•	1	ı		8.0	12 *
Silicon - 31	4.6	6.7	7.5	8.3	9.9	6.9	7.1	4.9	8.2	5.5
Phosphorus - 32	1	90.0	0.013	0.37	•	•	0.56	0.63	0.3	0.37



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	EFFLUENT WATER
V (Cont.)	TS OF REACTOR
TABLE	OR CONSTITUENTS
	OF MAJOR
	ACTIVIT

Sample Location	100-F	100-F	100-F	100-F	100-F	100-F	100-F	100-F
Sampling Date	1-3-52	2-6-52	2-27-52	3-27-52		5-6-52	5-56-52	6-12-52
Sampling Time	0630	0660	9060	9060	6260	0925	0935	0860
Total Beta Activity Density units of 10-3 uc/cc	1.9	2.5	2.3	3.0	†• †	2.7	3.5	2.9
& Total Beta Activity								
Manganese - 56	27	56	28	24	52	55	37	44
Sodium - 24	14	97	76	13	6	21	9.9	30
Copper - 64	97	14	18	7.4	7.7	12	1.6	9.1
Arsenic - 76	94.0	4.2	3.5	5.5	2.3	3.9	2.2	3.5
Rare Earths + Y	ı	7.3	7.5	7.1		1.9	6.9	9.6
Silicon - 31	6.8	7.3	9.6	3.3	4.2	9.9	8.2	п
Phosphorus - 32	91.0	14.0	0.51	•	0.067	0.51	0.19	0.36



0.16

0.05

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	ACI	IVITY OF	MA JOR CON	ACTIVITY OF MAJOR CONSTITUENTS OF REACTOR EFFLUENT WATER	Cont.)	OR EFFLUE	NT WATER			
Sample Location	100-H	100-H	100-н	100-H	100-H	100-1	100-H	100-H	100-H	100-H
Sampling Date	1-10-51	1-16-51	1-29-51	2-15-51	3-19-51	3-28-51	4-3-51	4-10-51	4-23-51 5-16-51	5-16-51
Sampling Time	040	9460	0850	0160	0915	0915	0935	5420	1000	0460
Total Beta Activity Density, units of 10-3 uc/cc	1.9	1.8	1.8	1.6	2.3	S.	2.6	2.1	2.0	2.5
\$ Total Beta Activity										
Manganese - 56	27	ซ	15		28	56	25	33	25	18
Sodium - 24	23	7.1	17	1	7,5	21	7.4	18	. 21	8.9
Copper - 64	12	27	9.3	ı	32	91	23	88		. 81
Arsenic - 76	4.1	1	.3.8	ı	2.5	7. 7	2.1	5.2	1.1	0.5
Rare Earths + Y		•		. 4.5	5.6	1.5	•	3.4	3.3	. 1
Silicon - 31	1	•	ı	•	,	1	•	1		,
Phosphorus - 32	ı	•	0.87	1	0.42	0.09	. 1	0.05	,	0.16



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	н-о	-18-51	30	6.			١٥.	

ACTIVITY OF MAJOR CONSTITUENTS OF REACTOR EFFLUENT WATER

Sample Tocation	100-H	100-H	100-н	100-H	100-н	100-H	100-H	100-н	100-H	100-H
Sampling Date	6-5-51	6-25-51	7-9-51	7-25-51	9-5-51	9-20-51	10-2-51	10-22-51	10-22-51 11-28-51 12-18-5	12-18-5
Sampling Time	0935	0360	0935	9060	0850	0830	0915	0350	0925	0630
Total Beta Activity Density, units of 10-3 uc/cc	2.1	1.9	1.8	1.6	1.8	2.0	1.3	1.6	2.2	1.9
% Total Beta Activity										
Manganese - 56	5	27	23	77	16	50	1 ¢	15	16	21
no - mil pos	17	16	15	19	17	15	12	† 1	12	91
de la composición del composición de la composic	15	56	31	21	33	34	25	34	82	ជ
Copper = 04	۲. ۱	0.5	0.2	0.5	4.0	٥ . د	7.0	1.0	6.0	1.0
A CHAPTER OF THE		1	•	1	•	ı	ı	•	13 *	ı
Rare parting + 1	1	9.0	6.5	4.5	4.5	6.5	5.8	5.0	6.2	8.5
Phosphorus - 32	0.25	. 1	0.05	1	ı	•	4.0	ı	0.90	0.73



0.35

0.23

44.0

0.39

0.51

0.55

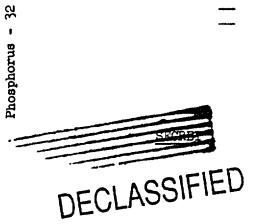
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ACTIVITY OF MAJOR CONSTITUENTS OF REACTOR EFFLUENT WATER

Sample Location	100-H	H-00T	H-001	H-001	H-001	100-H	100-H	100-11
Sampling Date	1-7-52	1-14-52	2-20-52	3-10-52	4-16-52	4-22-52	5-28-52	6-16-52
Sampling Time	0460	0660	0915	0915	0915	0660	0925	0915
Total Beta Activity Density, units of 10-3 uc/cc	1.2	1.9	2.2	2.0	2.7	2.5	2.0	1.8
% Total Beta Activity								
Manganese - 56	23	1,4	7.6	ָּד ֹ	14	ಬ	25	19
Sodium - 24	19	13	16	16	13	12	13	15
Copper - 64	745	54	27	37	56	53	59	23
Arsenic - 76	7.3	2.7	3.7	1	2.5	2.6	٥٠.	7.1
Rare Earths + Y	1	ı	ជ	8.3	5.0	9.4	5.5	8.4
Silicon - 31	7.5	6.5	6.2	6.4	5.1	4.5	ជ	15



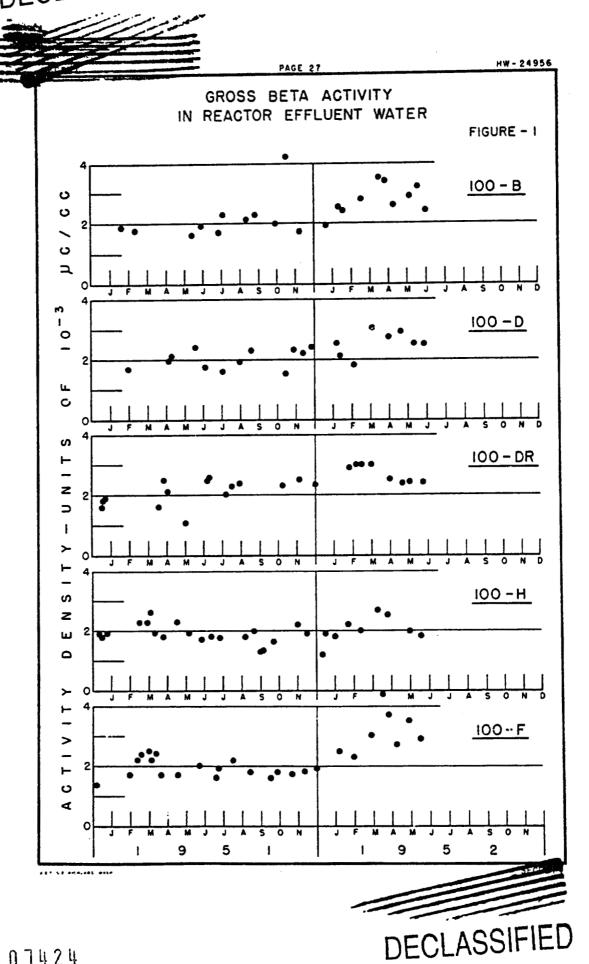




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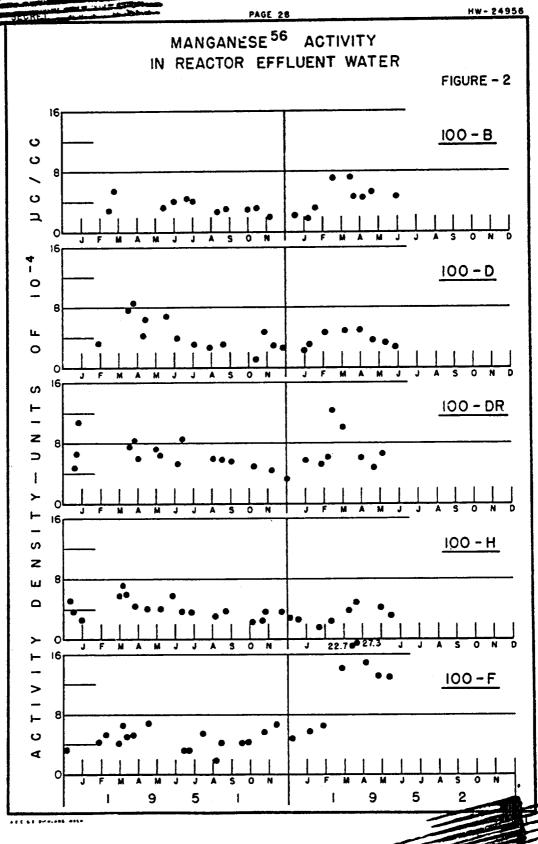
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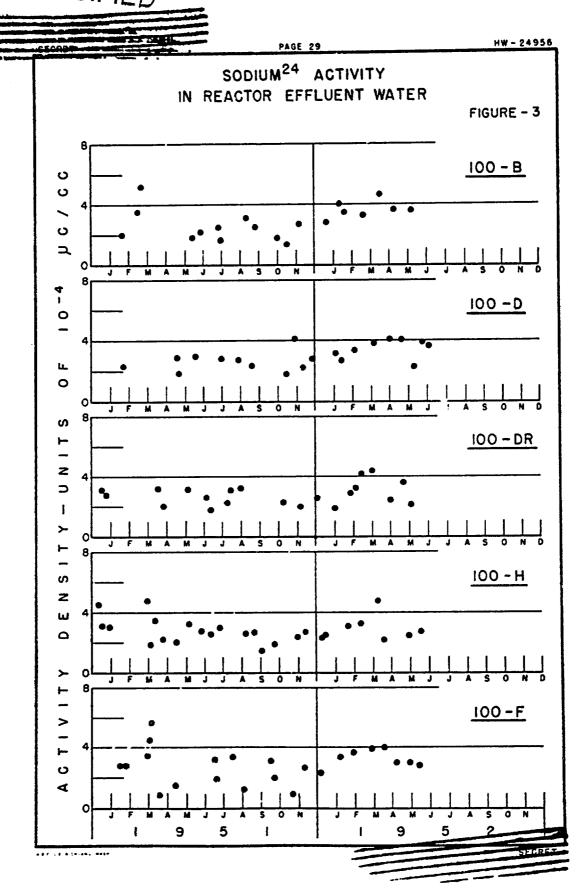


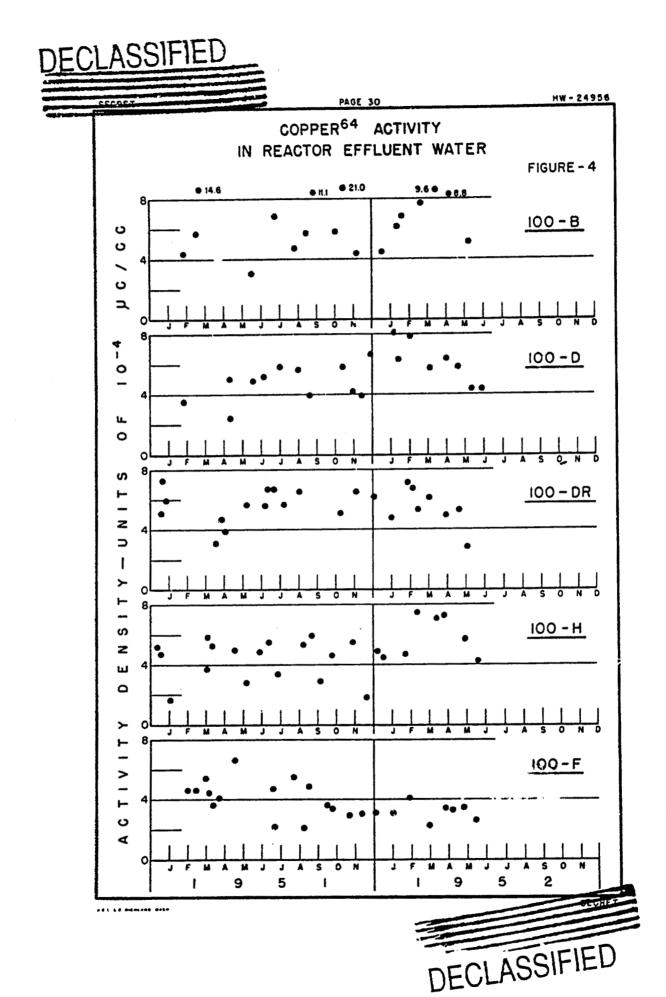


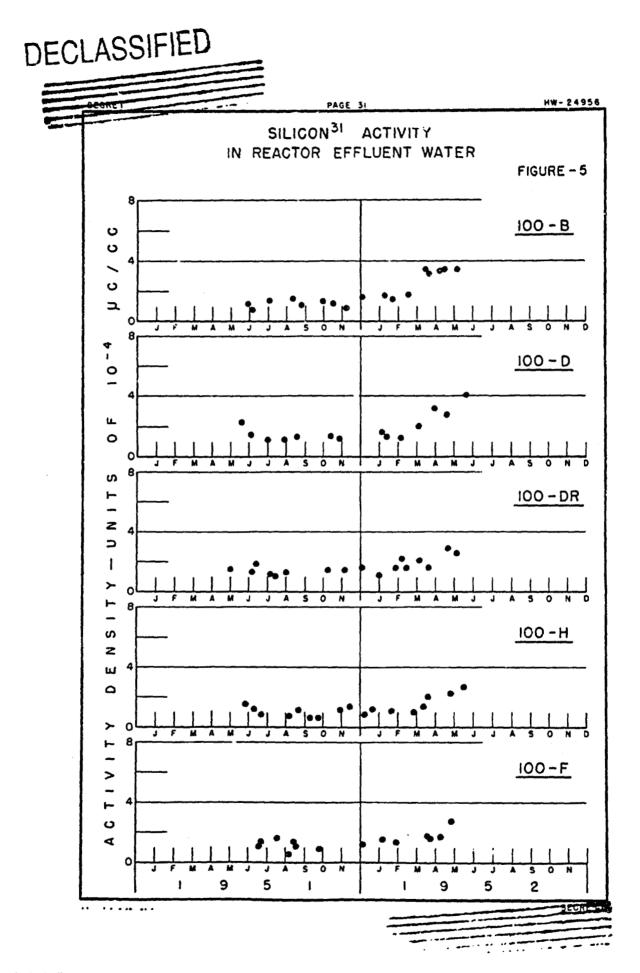


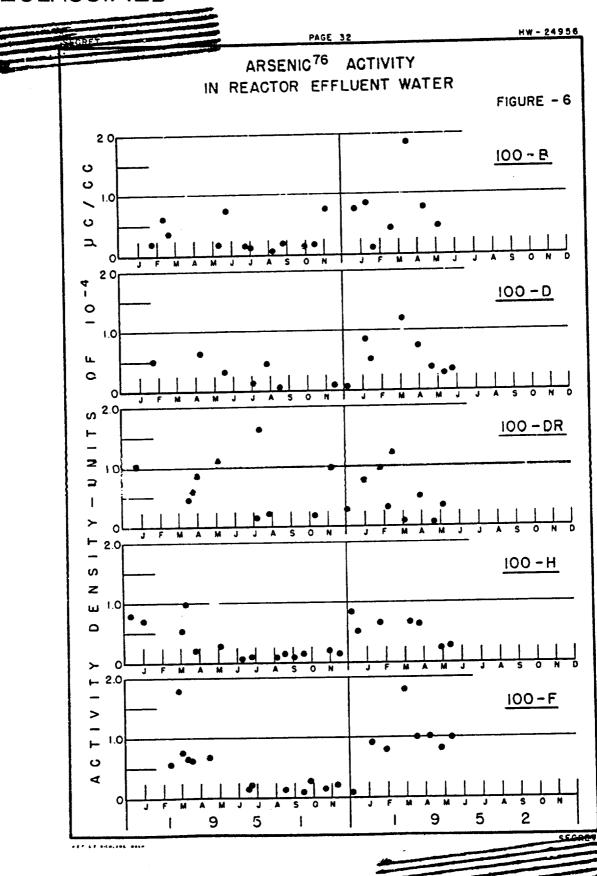
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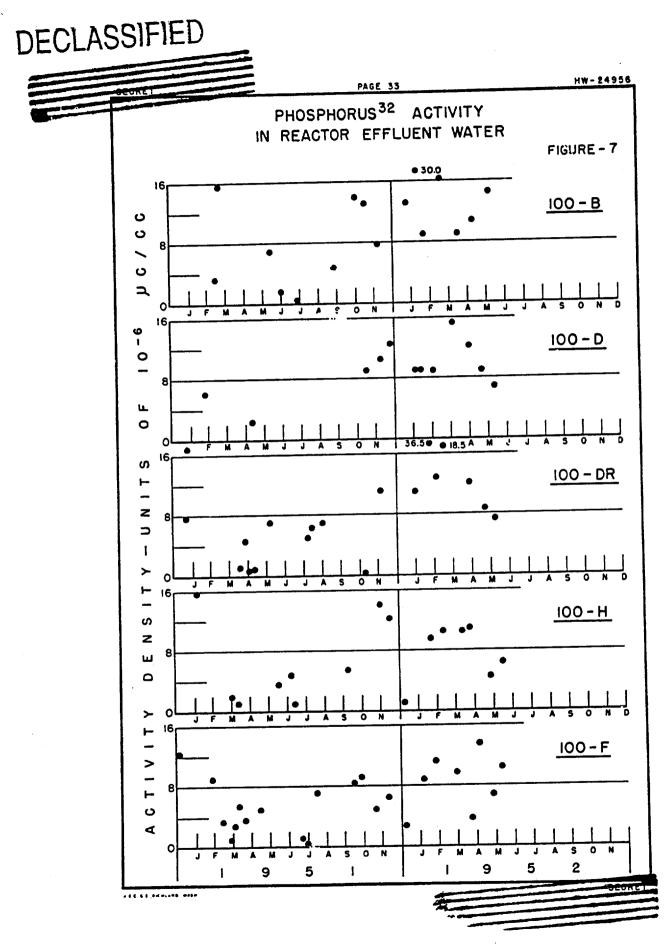














APPENDIX

DETERMINATION OF STRONTIUM AND BARIUM Fuming Nitric Acid Method

PRINCIPLES AND LIMITATIONS OF METHOD:

This procedure is based upon the solubility of calcium nitrate in concentrated nitric and while barium and strontium nitrates are not appreciably soluble. This procedure gives an excellent separation if the calcium present is not more than 0.1 gram. Chemical yield is approximately 80%. The time required is about two hours.

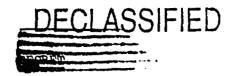
REAGENTS.

- 1. Carriers (Ag, Cu, Fe, La, Sr, Ba, Ca, and Na), 10 mg/ml standardized.
- 2. Nitric Acid, fuming.
- 3. Ammonium Hydroxide, c.p.
- 4. Hydrogen Sulfide, gas.
- 5. Sodium Carbonate, saturated solution.
- 6. Ammonium Bichromate, 100 g/l solution.
- 7. Ammonium Oxalate, saturated solution.
- 8. Ammonium Acetate, 3N solution.

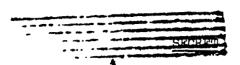
PROCEDURE:

- 1. Transfer 100 ml of reactor effluent water to a 250 ml beaker.
- 2. Add 2.00 ml of Sr and Ba and about 2 ml of Ag, Cu, Fe, La, Ca, and Na.
- 3. Make ammoniacal and precipitate with hydrogen sulfide.
- 4. Centrifuge and save supernate. Discard precipitate.
- 5. Bring solution to boil and acidify. Boil until hydrogen sulfide is gone.
- 6. Add saturated sodium carbonate solution until harin and cool.
- 7. Filter through #42 filter paper, wash with 1% sodium carbonate solution, and discard filtrate.





- 8. Cautiously dissolve precipitate through the paper with dilute nitric acid and wash thoroughly with water.
- 9. Evaporate to 5 ml.
- 10. Add 30 ml of fuming nitric acid. Cool and centrifuge.
- 11. Decant solution and discard.
- 12. Dissolve precipitate in 2 ml of water and add 15 ml of fuming nitric acid. Cool and centrifuge.
- 13. Dissolve precipitate in 20 ml of water.
- 14. Add 5 ml of 3N ammonium acetate solution and bring to boil.
- 15. Add 5 ml of ammonium bichromate dropwise and cool.
- 16. Centrifuge. Save supernate and wash precipitate until washings are colorless. Add washings to supernate.
- 17. Dissolve precipitate in 2N nitric acid and re-precipitate with ammonium hydroxide.
- 18. Centrifuge. Discard supernate and wash once with water.
- 19. Transfer the barium chromate precipitate to a stainless steel plate and dry. Count at hourly intervals.
- 20. Add 10 ml of ammonium oxalate solution to the supernate in step (16).
- 21. Bring to boil and make ammoniacal.
- 22. Cool, centrifuge, and discard supernate.
- 23. Wash three times with water.
- 24. Count at hourly intervals. Transfer the strontium oxalate precipitate to a stainless steel plate and dry.





DETERMINATION OF SODIUM Group Separations Method

PRINCIPLE AND LIMITATIONS OF METHOD:

Sodium²⁴, which has a half-life of 14.9 hours, constitutes approximately twenty percent of the total activity of reactor effluent water.

In this procedure, the analytical Groups I, II, and III are removed as sulfides from a basic solution and Group IV is removed as the oxalate. The solution is then evaporated to dryness and ignited to remove ammonium salts. The residue is taken up with water, filtered, acidified and plated.

THIS PROCEDURE HAS BEEN TESTED ONLY ON REACTOR EFFLUENT WATER.

REAGENTS:

- 1. Ammonium Hydroxide, c.p. concentrated.
- 2. Ammonium Oxalate Solution, saturated aqueous.
- 3. Carriers (silver, copper, iron, lanthanum, calcium, and sodium), 10.
- 4. Hydrogen Sulfide, gas.
- 5. Nitric Acid, c.p. concentrated.

PROCEDURE:

- Transfer 100 ml of reactor effluent water to a 250 ml beaker. Add
 2.00 ml of sodium carrier and 2 ml of silver, copper, iron, lanthanum,
 and calcium carriers.
- 2. Add 1 ml of ammonium hydroxide and pass in hydrogen sulfide for two minutes.
- 3. Centrifuge and decant the supernate through a #40 Whatman filter paper.
- 4. Add > ml of ammonium oxalate solution to the filtrate and heat to boiling.
- 5. Centrifuge, depart the supernate through a #40 Whatman filter paper, and evaporate the filtrate to dryness.
- 4. Ignite the beaker and contents over a Meker burner until all of the ammonium salts are removed.





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- 7. Add 20 ml of distilled water and heat to boiling.
- 8. Filter, wash the paper with hot water and collect the filtrate and washings in a 100 ml beaker.
- 9. Add 2 ml of nitric acid, evaporate to a volume of 3 to 4 ml, and transfer to a one inch stainless steel plate.
- 10. Dry under an infra-red lamp. Count at hourly intervals.





DETERMINATION OF TOTAL RARE EARTHS AND YTTRIUM

Ceric Fluoride Method

PRINCIPLE AND LIMITATIONS OF METHOD:

The rare earths are precipitated as fluoride using a cerium carrier. The zirconium is removed by complexing with the hydrofluoric acid. Barium and strontium are removed by precipitation of the rare earths as hydroxides in the presence of a strontium holdback carrier. The hydroxide precipitate is then plated and counted.

This method was adapted from a fission product procedure and was not designed primarily for the analysis of reactor effluent water.

REAGENTS:

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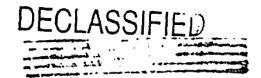
- 1. Ammonium Hydroxide, concentrated.
- 2. Boric Acid Solution, saturated, aqueous.
- 3. Carriers (cerium, strontium), 10 mg/ml standardized.
- 4. Hydrochloric Acid, 6N.
- 5. Hydrofluoric Acid, 27N.
- 6. Nitric Acid, c.p. concentrated.
- 7. Nitric Acid, 4N.
- 8. Sodium Hydroxide, 24%

Dissolve 240 g c.p. sodium hydroxide in 1000 ml of water.

PROCEDURE:

- Place a 50 ml sample of reactor effluent water (concentrate if necessary) in a 100 ml lusteroid test tube.
- 2. Add 2.00 ml of cerium carrier, 4 ml of zirconium carrier and 15 ml of concentrated nitric acid.
- 3. Add 2 ml concentrated hydrofluoric acid, stir and centrifuge.
- 4. Decant supernate and dissolve the precipitate in 2 ml saturated boric





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acid solution and 1 ml of concentrated nitric acid. Add 2 ml zirconium carrier.

- Dilute to 10 ml, add 2 ml concentrated hydrofluoric acid, stir and centrifuge.
- 6. Decant supernate, dissolve the precipitate in 2 ml of saturated boric acid solution and 1 ml of acentrated nitric acid.
- 7. Make the solution basic with sodium hydroxide, centrifuge, and wash the precipitate twice with water.
- 8. Dissolve the precipitate in 1 to 2 ml 6N hydrochloric acid and add 2 ml strontium carrier.
- 9. Dilute to 15 ml, make the solution basic with ammonium hydroxide, and centrifuge.
- 10. Decant the supernate, dissolve the precipitate in 1 to 2 ml 6 m hydrochloric acid. Dilute to 15 ml.
- ll. Make the solution basi with ammonium hydroxide, centrifuge, wash the precipitate twice with water and mount on a stainless steel plate.

 Ignite. Measure the counting rate hourly.

